

# ***PROline promag 53*** **Division 1**



**Fieldbus  
Foundation**



Ex documentation for the BA 051D and BA 052D operating instructions according to FACTORY MUTUAL standards



Ex documentation for the BA 051D and BA 052D operating instructions according to CANADIAN STANDARDS ASSOCIATION



**Endress + Hauser**

The Power of Know How





# PROline promag 53 Division 1

## Ex documentation for the BA 051D and BA 052D operating instructions

according to FACTORY MUTUAL standards



Example: **XP / I / 1 / ABCD**

### Type of Protection

XP	Explosionproof
IS	Intrinsically Safe Apparatus
AIS	Associated Apparatus with Intrinsically Safe Connections
ANI	Nonincendive Field Wiring Circuit
PX, PY, PZ	Pressurized
APX, APY, APZ	Associated Pressurization Systems/Components
NI	Nonincendive
DIP	Dust-Ignitionproof
S	Special Protection

### Class

I	Class I (Gas)
II	Class II (Dust)
III	Class III (Fibre)

### Division

1	Division 1
2	Division 2

### Group

FM / NEC	Gases, vapours and dusts (Examples)	Min. ignition temperature [ $\mu$ J]
A	Acetylene, carbon disulfide (Class I)	0.02
B	Hydrogen, ethyl nitrate (Class I)	0.02
C	Ethylene, isoprene (Class I)	0.06
D	Acetone, ethane, benzene, ethanoic acid, gasolines, diesel oil, aircraft fuel, methane, heating oil, crude oil, hexane, ether (Class I)	0.18
E	Metallic powder (Class II)	
F	Coal dust (Class II)	
G	Mill dust (Class II) Textile fibres (Class III)	

### Temperature Class

FM 3611	Maximum surface temperature	
T1	842 °F	450 °C
T2	572 °F	300 °C
T2A	536 °F	280 °C
T2B	500 °F	260 °C
T2C	446 °F	230 °C
T2D	419 °F	215 °C
T3	392 °F	200 °C
T3A	356 °F	180 °C
T3B	329 °F	165 °C
T3C	320 °F	160 °C
T4	275 °F	135 °C
T4A	248 °F	120 °C
T5	212 °F	100 °C
T6	185 °F	85 °C

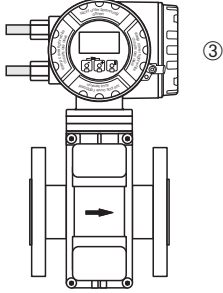
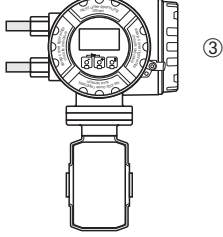
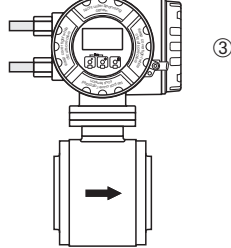
Factory Mutual



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Hazardous area		Safe area
Division 1 / Zone 1	Division 2 / Zone 2	
<p>Promag 53 P = DN 1/2"...12" W = DN 1"...12"</p> 		
<p>Promag 53 H = DN 1/12"...1"</p> 	<p>Promag 53 H = DN 1 1/2"...4"</p> 	
Division 1 / Zone 1	Division 2 / Zone 2	
Hazardous area		Safe area

F06-53xxxZZ-16-xx-xx-en-000

- Promag 53 FOUNDATION Fieldbus flow measuring system in:  
XP-IS-DIP / I,II,III / 1 / ABCDEFG/T5-T3C  
and  
XP-IS / I / 1 / IIC / T5-T3C
- For ambient and fluid temperature ranges, and temperature class, see Page 3.

③ Transmitter terminal compartment (XP version) power supply/bus cable

## Temperature tables

### Measuring system Promag 53 (compact version)

<i>at <math>T_a = 104\text{ }^\circ\text{F}</math></i>		Max. medium temperature [ $^\circ\text{F}$ ] in					
		T5	T4A	T4	T3C	T2	T1
<b>Promag H</b>	DN 1/12"...4"	122	230	266	302	302	302
<b>Promag P</b>	DN 1"...8" (PFA lining)	122	230	266	302	302	302
<b>Promag P</b>	DN 1/2"...12" (PTFE lining)	122	230	266	266	266	266
<b>Promag W</b>	DN 1"...12" (polyurethan lining)	122	140	140	140	140	140
<b>Promag W</b>	DN 2 1/2"...12" (hard-rubber lining)	122	176	176	176	176	176

<i>at <math>T_a = 113\text{ }^\circ\text{F}</math></i>		Max. medium temperature [ $^\circ\text{F}$ ] in					
		T5	T4A	T4	T3C	T2	T1
<b>Promag H</b>	DN 1/12"...4"	122	230	266	266	266	266
<b>Promag P</b>	DN 1"...8" (PFA lining)	122	230	266	266	266	266
<b>Promag P</b>	DN 1/2"...12" (PTFE lining)	122	230	266	266	266	266
<b>Promag W</b>	DN 1"...12" (polyurethan lining)	122	140	140	140	140	140
<b>Promag W</b>	DN 2 1/2"...12" (hard-rubber lining)	122	176	176	176	176	176

<i>at <math>T_a = 122\text{ }^\circ\text{F}</math></i>		Max. medium temperature [ $^\circ\text{F}$ ] in					
		T5	T4A	T4	T3C	T2	T1
<b>Promag H</b>	DN 1/12"...4"	122	230	230	230	230	230
<b>Promag P</b>	DN 1"...8" (PFA lining)	122	230	230	230	230	230
<b>Promag P</b>	DN 1/2"...12" (PTFE lining)	122	230	230	230	230	230
<b>Promag W</b>	DN 1"...12" (polyurethan lining)	122	140	140	140	140	140
<b>Promag W</b>	DN 2 1/2"...12" (hard-rubber lining)	122	176	176	176	176	176



Note:

At the specified medium temperatures, the equipment is not subjected to temperatures impermissible for the temperature class in question.

## Approvals

No. / approval type	Description
J. I. 3002554  (See Page 5 for notes on special conditions)	for the electric flow measuring system Promag 53 FOUNDATION Fieldbus  <b>Identification:</b> see below

Measuring system Promag 53 FOUNDATION Fieldbus (compact version)	
Promag 53***_*****	G = FOUNDATION Fieldbus, intrinsically safe K = FOUNDATION Fieldbus
Promag 53 H DN 1/12"...4":	<b>XP-IS-DIP / I,II,III / 1 / ABCDEFG / T5-T3C; XP-IS / 1 / 1 / IIC / T5-T3C</b>
Promag 53 P DN 1/2"...12":	<b>XP-IS-DIP / I,II,III / 1 / ABCDEFG / T5-T3C; XP-IS / 1 / 1 / IIC / T5-T3C</b>
Promag 53 W DN 1"...12":	<b>XP-IS-DIP / I,II,III / 1 / ABCDEFG / T5-T3C; XP-IS / 1 / 1 / IIC / T5-T3C</b>

## Notified body

The Promag measuring system was tested for approval by the following named entity:

FM: Factory Mutual Research

## Special conditions

1. Install per National Electrical Code ANSI/NFPA 70.
2. Control room equipment shall not use or generate more than 250 V rms.
3. The specified temperature class in conjunction with the ambient temperature and the medium temperature must be in compliance with the tables on Page 3.
4. Use of the devices is restricted to mediums against which the process-wetted materials are adequately resistant.
5. Use supply wires suitable for 41 °F above ambient temperature, but at least for 176 °F.
6. Devices connected to terminals Nos. 20 to 27 of the Promag 53 FOUNDATION Fieldbus transmitter must be rated for  $U_m = 260$  V and  $I_m = 500$  mA: it is impermissible to connect devices with higher ratings to these terminals.  
(Does not apply to Promag 53\*\*\*-\*\*\*\*\*G with intrinsically safe output circuit).

## General warnings



Warning:

- Installation, connection to the electricity supply, commissioning and maintenance of the devices must be carried out by qualified specialists trained to work on Ex-rated devices.
- Compliance with national regulations relating to the installation of devices in potentially explosive atmospheres is mandatory, if such regulations exist.
- Open the device only when it is de-energized (and after a delay of at least 10 minutes following shutdown of the power supply).
- The housing of the Ex-rated transmitter can be turned in 90° steps. Whereas the non-Ex version has a bayonet adapter, however, the Ex version has a thread. Recesses for centering the worm screw are provided to prevent inadvertent movement of the transmitter housing.  
It is permissible to turn the transmitter housing through a maximum of 180° during operation (in either direction), without compromising explosion protection.  
After turning the housing the worm screw must be fastened again.
- The screw cap has to be removed before the local display can be turned, and this must be done with the device de-energized (and after a delay of at least 10 minutes following shutdown of the power supply).

## Electrical connections

### Power supply connection

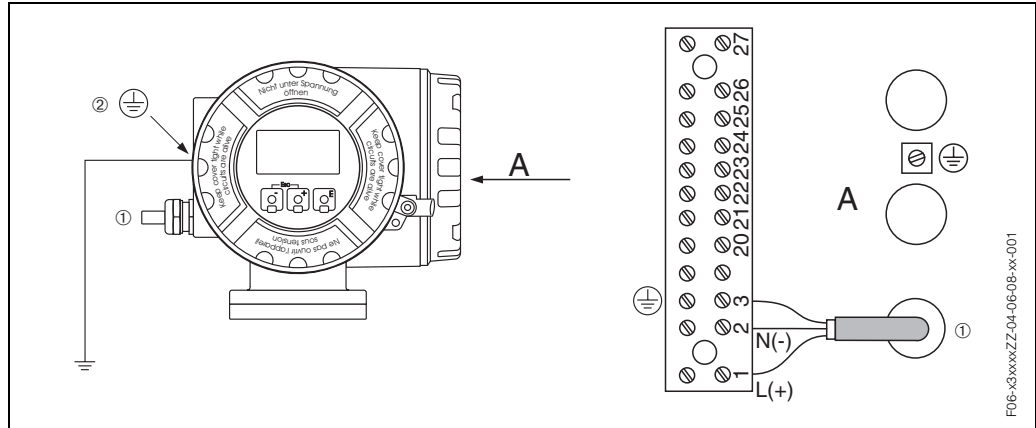


Fig. 1: ① = Power supply cable  
 ② = Ground terminal for potential equalisation  
 A = View A

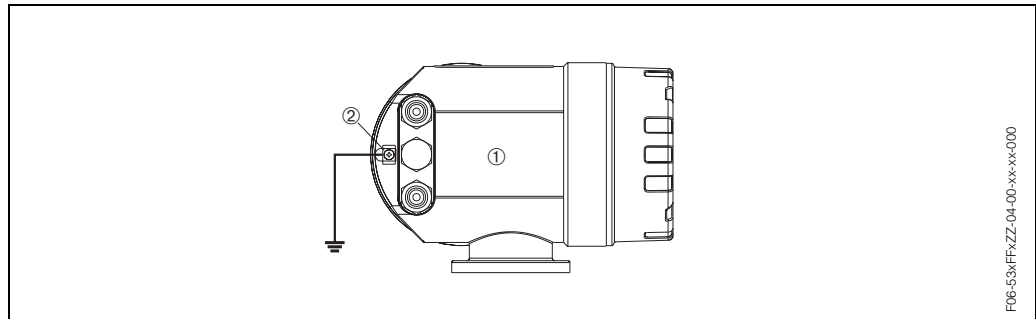


Fig. 2: Ground terminal for potential equalisation



#### Caution:

- The transmitter ① is to be securely connected to the potential equalization system using the screw terminal ② on the outside of the transmitter housing.

The table below contains the values that are identical for all versions, irrespective of the type code.

### Transmitter Promag 53

Terminals	1	2	3
	L (+)	N (-)	
Designation	Power supply ①		Protective earth
Functional values	AC: U = 85...260 V or AC: U = 20...55 V or DC: U = 16...62 V  Power consumption: 15 VA / 15 W		Caution: Follow ground network requirements for the facility
Intrinsically safe circuit	no		
U <sub>max</sub> =	260 V AC		



**Input/output circuit**

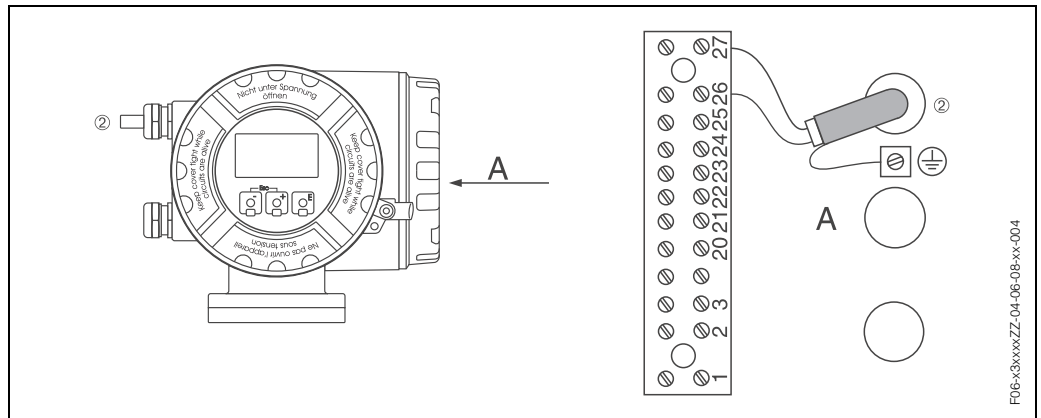


Fig. 3: ② = Bus cable (FOUNDATION Fieldbus)  
A = View A



**Note:**

The table below contains the values which depend on the type code (type of device). Always remember to compare the type code in the table with the code on the nameplate of your device.

**Transmitter Promag 53\*\*\*-\*\*\*\*\*G**

Terminals	20	21	22	23	24	25	26	27
	+	-	+	-	+	-	+	-
Designation							FOUNDATION Fieldbus ②	
Functional values							$U_B = 9...32 \text{ V DC}$ $I_B = 12 \text{ mA}$	
Intrinsically safe circuit							EEx ia	
$U_i =$							30 V DC	
$I_i =$							500 mA	
$P_i =$							5.5 W	
$L_i =$							10 $\mu\text{H}$	
$C_i =$							5 nF	

**Transmitter Promag 53\*\*\*-\*\*\*\*\*K**

Terminals	20	21	22	23	24	25	26	27
	+	-	+	-	+	-	+	-
Designation							FOUNDATION Fieldbus ②	
Functional values							$U_B = 9...32 \text{ V DC}$ $I_B = 12 \text{ mA}$	
Intrinsically safe circuit							no	
$U_{max} =$							260 V AC	
$I_{max} =$							500 mA	

## Service adapter

The service adapter is exclusively for connection to E+H approved service interfaces.



Warning:

It is not permissible to connect the service adapter in explosive atmospheres.

## Device fuse



Warning:

Use only fuses of the following types; the fuses are installed on the power supply board:

- Voltage 20...55 V AC / 16...62 V DC:  
 fuse 2.0 A slow-blow, disconnect capacity 1500 A  
 (Schurter, 0001.2503 or Wickmann, Standard Type 181 2.0 A)
- Voltage 85...260 V AC:  
 fuse 0.8 A slow-blow, disconnect capacity 1500 A  
 (Schurter, 0001.2507 or Wickmann, Standard Type 181 0.8 A)

## Cable entries

For number reference see the figure on Page 2.

- ③ *Cable entries for the transmitter terminal compartment (XP version)  
 power supply / bus cable: (Promag 53\*\*\*-\*\*\*\*N\*\*\*\*\*)  
 Thread for cable entries 1/2" NPT.*

Make sure that the XP cable entries are secured to prevent them from working loose.

## Technical data

### Dimensions wall-mount housing

Weight approx. 14.8 lbs

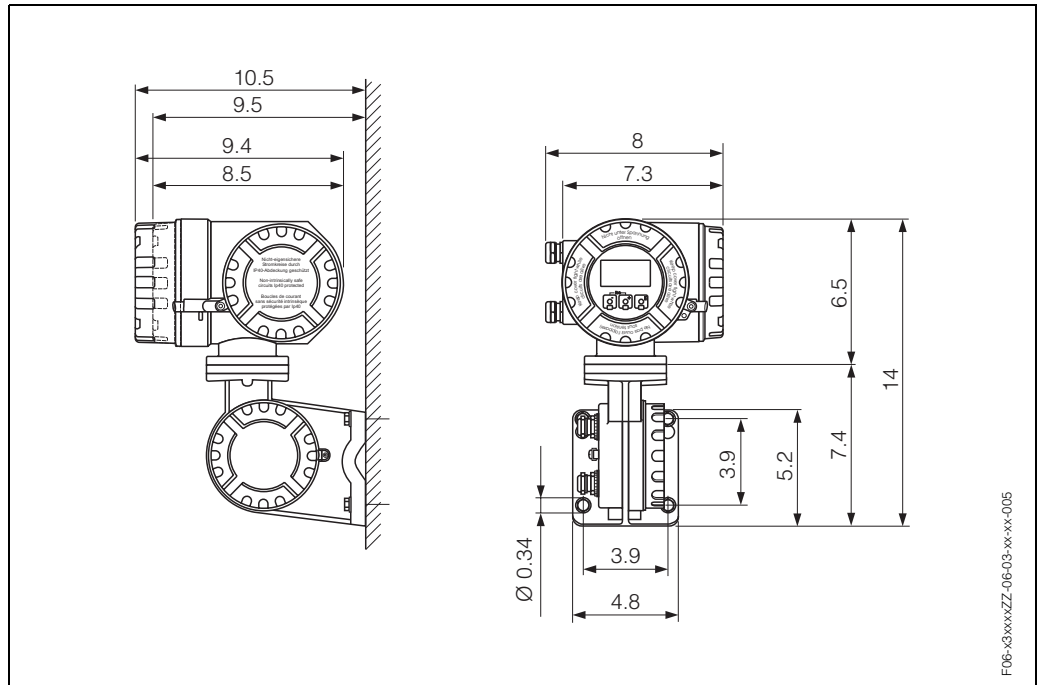


Fig. 4: Dimensions wall-mount housing

## Bus cable for FOUNDATION Fieldbus

The Fieldbus FOUNDATION defines four different types of cable in the specification creating the physical transmission layer (FF-816) which is analogous to IEC 61158-2. A two-core cable is always specified.

The electrical data has not been specified but determines important characteristics of the design of the fieldbus, such as distances bridged, number of participants, electromagnetic compatibility, etc.

Two of the four cable types in the standard are specified in the following table.

	<b>Cable type A (reference)</b>	<b>Cable type B</b>
<i>Cable construction</i>	twisted pair, shielded	one or more twisted pairs, fully shielded
<i>Core cross-section (nominal)</i>	0.8 mm <sup>2</sup> (AWG 18)	0.32 mm <sup>2</sup> (AWG 22)
<i>Loop resistance (direct current)</i>	44 Ω/km	112 Ω/km
<i>Impedance at 31.25 kHz</i>	100 Ω ± 20%	100 Ω ± 30%
<i>Attenuation constant at 39 kHz</i>	3 dB/km	5 dB/km
<i>Capacitive unsymmetry</i>	2 nF/km	2 nF/km
<i>Envelope delay distortion (7.9...39 kHz)</i>	1.7 μs/km	**
<i>Degree of voltage of shielding</i>	90%	**
<i>Max. bus segment length (inc. spur lines)</i>	1900 m (6234 ft)	1200 m (3937 ft)

Tab. 1: Cable types

We recommend the use of cables meeting the minimum requirements of type A as transmission medium, particularly for the installation of new systems. The recommended network expansion is made up of the length of the main cable and the length of all spurs. The line between distribution box and field device is described as a spur. The maximum length of a spur depends on the number of spurs (> 1 m [3 ft]). A maximum of four field devices can be connected to a spur.

<b>Number of spurs</b>	<b>1...12</b>	<b>13...14</b>	<b>15...18</b>	<b>19...24</b>	<b>25...32</b>
Max. length per spur	120 m (394 ft)	90 m (295 ft)	60 m (197 ft)	30 m (98 ft)	1 m (3 ft)

Tab. 2: Table of possible spur line lengths

The following table shows examples of FOUNDATION Fieldbus bus cables (type A) from various manufacturers.

<b>Supplier</b>	<b>Model</b>	<b>Order number</b>
Belden	3076	–
Kerpen	FB-02YS (St+C) Y-FL	74220001 (light blue) 74220004 (black)
Siemens	SIMATIC NET bus cable	6XV1830-5AH10 (light blue) 6XV1830-5BH10 (black)

Tab. 3: Possible cable suppliers

**Bus termination**

The start and end of each fieldbus segment are always to be terminated with a bus terminator.

- In the case of a branched bus segment the measuring device furthest from the segment connector represents the end of the bus.
- If the fieldbus is extended with a repeater then the extension must also be terminated at both ends.

**Selecting and connecting components**

The FOUNDATION Fieldbus allows several devices from different manufacturers to be generally connected to a bus segment. When selecting components for use in areas with an explosion risk only components marked as intrinsically safe, explosion-protected electrical equipment or as intrinsically safe associated electrical equipment may be used. When combining different fieldbus devices and fieldbus components, in addition to functional considerations, technical safety factors must be considered if explosion protection is to be ensured.

**Implementation of intrinsic safety in the FOUNDATION Fieldbus H1**

The FOUNDATION Fieldbus H1 can be made intrinsically safe for use in areas with an explosion risk (EEx i). To do this, according to the FOUNDATION Fieldbus specification a suitable safety component must be installed (FF-816) between the safe area and the area with an explosion risk. The intrinsically safe bus segment can be supplied either by a non-intrinsically safe power supply with a safety barrier downstream or by a fieldbus power supply with an intrinsically safe output.

It is recommended that the cable shielding be grounded at both ends (refer to Fig. 6, Page 14).

Installation example of a galvanic isolator with bus feed:

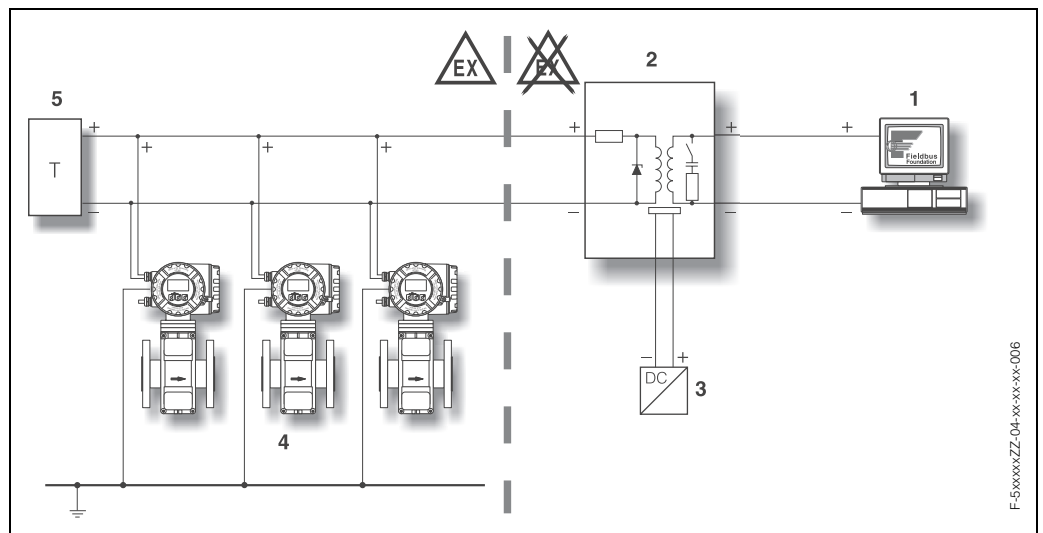


Fig. 5: Typical embodiment of a galvanic isolator including fieldbus power supply

- 1 = DCS with integrated FOUNDATION Fieldbus H1 interface card
- 2 = fieldbus power supply: galvanic isolator
- 3 = fieldbus power supply
- 4 = Promag 53 bus devices for hazardous area
- 5 = terminator (T) = bus termination

## Proof of intrinsic safety

Proof of intrinsic safety for the intrinsically safe bus segment can be made by using one of the following models:

- Entity model
- FISCO model

Both models differ from one another by their consideration of the cable. While the FISCO model considers the transmission line as distributed inductance and capacitance, the basis of this consideration for the Entity model is concentrated inductance and capacitance. The result of this is that lower quantities of power can be transmitted with the Entity model into the Ex area, and that the number of field devices that can be operated on a power repeater is therefore lower than with the FISCO model.

In the case of failure, instruments from different manufacturers can be exchanged when their safety-relevant data is taken into consideration. This data is: electrical parameters, device group and category, and the temperature class.

Both these models are briefly described in the following.

### The Entity model

The Entity model is based on the observation that the cable represents concentrated inductance and capacitance. The result is that less electrical power can be transmitted into the area subject to the risk of explosion when compared with the FISCO model.

The following conditions must be met in the safety according to the entity model considerations:

Field device Hazardous area	Mandatory	Power supply Safe area
Maximum voltage [U <sub>i</sub> ]	≥	Idle voltage of the safety element [U <sub>o</sub> ]
Maximum current [I <sub>i</sub> ]	≥	Short-circuit current [I <sub>o</sub> ]
Maximum power [P <sub>i</sub> ]	≥	[P <sub>o</sub> ]
Effective internal capacitance [C <sub>i</sub> ] + cable capacitance	≤	Maximum permitted external capacitance [C <sub>o</sub> ]
Effective internal inductance [L <sub>i</sub> ] + cable inductance	≤	Maximum permitted external inductance [L <sub>o</sub> ]

Tab. 4: General dependencies

In addition, the following measures must be taken:

- determine permissible explosion group for the bus segment
- determine all effective energy stores (L<sub>i</sub>, C<sub>i</sub>, capacitance and inductance per unit length)
- check locally supplied operating units for galvanic isolation
- harmonize temperature class and ambient temperature



Note:  
Configuration example see Page 16

## The FISCO model

The German Federal Physical-Technical Institute (PTB) has developed the FISCO model which was published in Report PTB-W-53 "Examination on Intrinsic Safety for Field Bus Systems".

The FISCO model makes possible the interconnection of intrinsically safe apparatus and one intrinsically safe associated apparatus, without having to have separate certification for respective connections.

The criteria for the intrinsic safety of an interconnection (bus segment) is given under the following interrelationships:

1. To transmit power and data, the bus system uses the physical configuration defined by IEC 61158-2. This is the case for FOUNDATION Fieldbus and the H1 bus.
2. Only one active source is permitted on a bus segment (here the power repeater). All other components work as passive current sinks.
3. The basic current consumption of a field device is at least 10 mA.
4.  $U_i$ ,  $I_i$  and  $P_i$  of the bus device  $\geq U_o$ ,  $I_o$  and  $P_o$  of the associated equipment (bus power supply).
5. Each instrument must fulfill the following requirement:  $C_i \leq 5$  nF,  $L_i \leq 10$   $\mu$ H
6. The permissible line length for EEx ia IIC applications is 1000 m (3280 ft).
7. The permissible spur length for Ex applications is 30 m (98 ft) per spur.
8. The transmission line that is used must conform to the following cable parameters:  
Resistor coating:  $15 \Omega/\text{km} < R' < 150 \Omega/\text{km}$   
Inductance coating:  $0.4 \text{ mH}/\text{km} < L' < 1 \text{ mH}/\text{km}$   
Capacitance coating:  $80 \text{ nF}/\text{km} < C' < 200 \text{ nF}/\text{km}$  (including the shield)
9. The bus segment must be terminated on both ends of the line with a terminal bus resistor. A terminal resistor is integrated into the power repeater so that an external bus terminator is only required on the other end. According to the FISCO model the fieldbus terminator must conform to the following limits:  
–  $90 \Omega < R < 100 \Omega$   
–  $0 \mu\text{F} < C < 2.2 \mu\text{F}$



Note:

Configuration example see Page 23

## Potential equalisation with shielding grounded at both ends

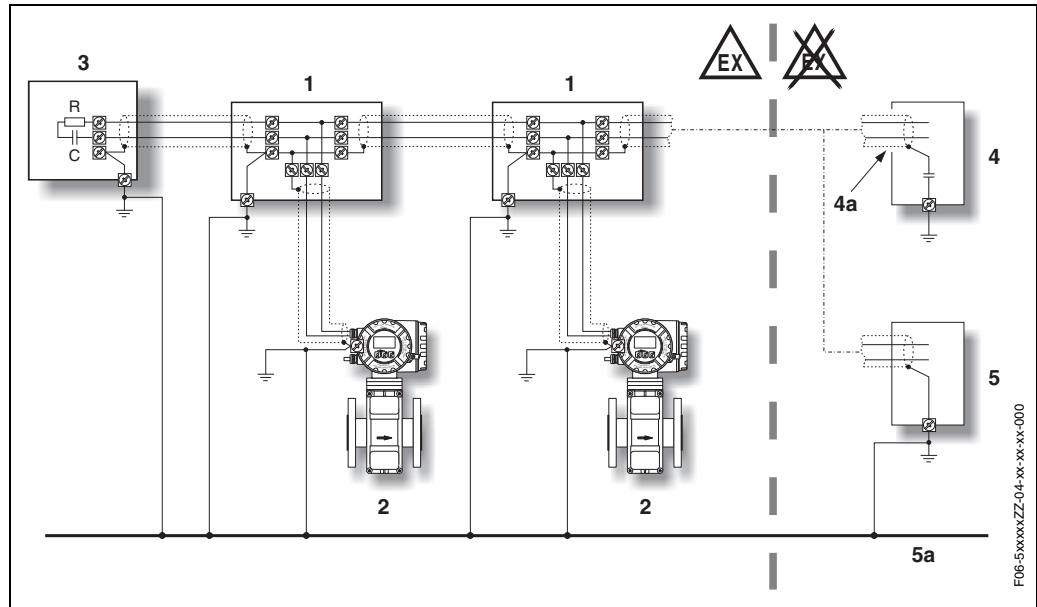


Fig. 6: Examples of the connection of potential equalisation lines

- 1 = distributor/T-box
- 2 = Promag 53 bus devices for hazardous area
- 3 = bus termination:  $R = 90 \dots 100 \Omega$ ,  $C = 0 \dots 2.2 \mu F$
- 4 = fieldbus power supply variant 4a
- 4a = shielding connected via capacitor
- 5 = fieldbus power supply variant 5a
- 5a = potential equalisation line led out

### Variant 4/4a:

With capacitive grounding of the shielding in the safe area the potential equalisation line does not need to be led out of the safe area.

Use small capacitors (e.g. 1 nF, 1500 V, dielectric strength, ceramic). The total capacitance connected at the shielding must not exceed 10 nF.

### Variant 5/5a:

Potential equalisation line is led out of the safe area.



## Network configuration for FOUNDATION Fieldbus H1

### General remarks

Various aspects are to be considered when configuring a FOUNDATION Fieldbus H1 segment and these must essentially be checked by two general types of considerations:

### Functional considerations

In the functional considerations, the characteristic of the technical function data laid down in IEC 61158-2 for the transmission technology of the FOUNDATION Fieldbus H1 and the physical network structure is checked. Here it must always be ensured that the total base currents of all bus participants does not exceed the maximum permissible feed current of the bus power supply and that the field devices are always supplied with a minimum bus voltage of 9 V.

### Technical safety considerations

For use of the FOUNDATION Fieldbus H1 in an area with an explosion risk, proof of intrinsic safety is to be provided for the entire bus segment by means of the technical safety considerations. Proof of intrinsic safety for the intrinsically safe bus segment can be made by using one of the following models:

#### *Entity model*

The safety considerations correspond to those in a conventional 4...20 mA measuring circuit. The only exception is that here more than one field device is supplied by the power supply. The safety considerations must result in the knowledge that the fieldbus power supply does not exceed the safety parameters ( $P$ -,  $U$ -,  $I$ -values) of the field devices and that the inductance and capacitance are within the permissible limits (example see Page 16).

#### *FISCO model*

If proof of intrinsic safety is made according to the FISCO model, it is to be verified that all components connected to the bus segment (field instruments, bus power supplies, bus terminator) are laid out according to the FISCO model. If this is the case, it must be proven that for each bus component the values of  $U_i$ ,  $I_i$  and  $P_i$  are greater or the same as the values of  $U_o$ ,  $I_o$  and  $P_o$  for the associated equipment (bus power supply). Example see Page 23.

### Configuration example for a FOUNDATION Fieldbus H1 segment

Based on the following example, the functional and safety-relevant considerations and calculations for the specification of a FOUNDATION Fieldbus H1 segment are carried out.

### Configuration example Entity model

Fig. 7 shows the typical structure and the associated components. The field devices are operated on a segment with the type of protection EEx ia. A galvanic isolator is used for the transition to the area with explosion risk. Field devices with a lower power consumption, such as the Cerabar S pressure gauge, are supplied via the two-wire line. In contrast, the Promag 53 as a four-wire device must be supplied via an local power supply.

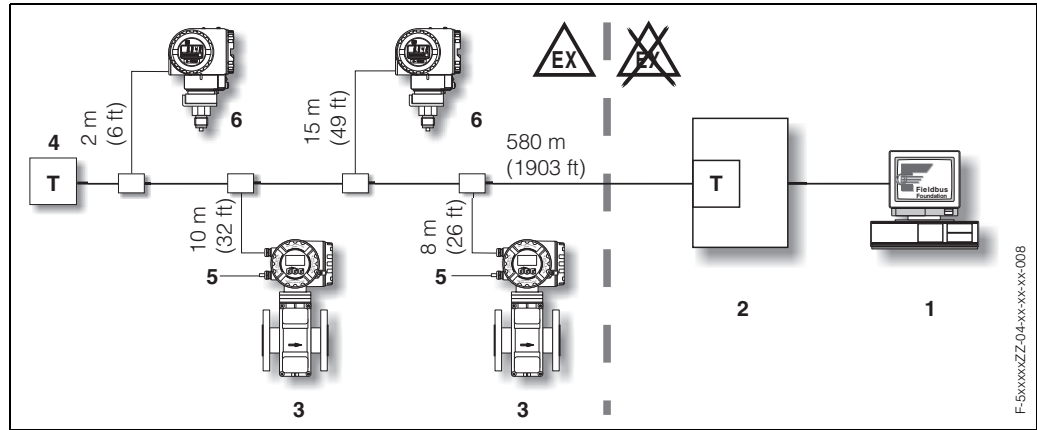


Fig. 7: Typical example of a bus connection with a fieldbus power supply of type MTL 5053

- 1 = DCS with integrated FOUNDATION Fieldbus H1 interface card
- 2 = fieldbus power supply, model MTL 5053
- 3 = Promag 53 bus devices for hazardous area
- 4 = terminator (T) = bus termination
- 5 = transducer supply
- 6 = Cerabar S bus devices for hazardous area

### Functional considerations

Using the following procedure the functional considerations checks whether the desired segment structure meets the basic requirements for transmission to the physical layer in IEC 61158-2.

Step 1 – compilation of the functional characteristic values of the fieldbus components

- Fieldbus power supply MTL 5053:
  - $U_S = 18.4 \text{ V}$
  - $I_S = 80 \text{ mA}$
  - $R_Q = 105 \Omega$  (source impedance)
- Fieldbus line:
  - Cable type A
  - $R_{WK} = 44 \Omega/\text{km}$  (effective resistance per unit length)
  - max. permissible cable length  $L_{perm.} = 1900 \text{ m}$  (6234 ft)
- Fieldbus device Promag 53:
  - $I_B = 12 \text{ mA}$  (basic current)
  - $U_B = 9...32 \text{ V}$  (perm. operating voltage)
  - $I_{FDE} = 0 \text{ mA}$  (fault current)
  - $I_{startup} = 0 (< I_B)$
- Fieldbus device Cerabar S:
  - $I_B = 10.5 \text{ mA}$  (basic current)
  - $U_B = 9...32 \text{ V}$  (perm. operating voltage)
  - $I_{FDE} = 0 \text{ mA}$  (fault current)
  - $I_{startup} = 0 (< I_B)$

### Step 2 – calculation of cable length and checking of network structure

The maximum cable length is always determined by the type of cable used. The actual cable length, which is made up of the length of the main cable and the length of the spur lines, must not exceed this value. The spur lines are also to be checked (refer to Table 2, Page 10). The following restrictions apply to the specification of the cable length and network structure:

- Where cable type A is used the cable length  $L_{perm.}$  may be max. 1900 m (6234 ft).
- Checking the spur line lengths (refer to Table 2, Page 10).

Calculation of actual cable length:

$$\begin{aligned}
 L_{SEG} &= L_{main.} + \Sigma L_{spurs} \\
 &= 580 \text{ m (1903 ft)} + 35 \text{ m (115 ft)} \\
 &= \underline{\underline{615 \text{ m (2018 ft)}}}
 \end{aligned}$$

Checking the conditions

Consideration	Condition met?
$L_{SEG} < L_{perm.}$	✓ Yes
$L_{spurs} < 120 \text{ m (394 ft)}$	✓ Yes

If one of the conditions is not met then the network structure must be revised.

### Step 3 – current calculation

The number of field devices that can be connected to the H1 segment depends on the fieldbus power supply selected (supply voltage and supply current) and the current consumption of the field devices. Thus, the number of devices that can be connected is reduced if a field device consumes a basic current of more than 10 mA, e.g. 20 mA. By adding up the basic currents  $I_B$  of the field devices plus the response current in the event of a fault  $I_{FDE}$  for the FDE (**F**ault **D**isconnect **E**lectronics) and the current for the data modulation  $I_{MOD}$  (+9 mA) you can determine the minimum supply current that the fieldbus power supply must supply.

If, on switching on the device, the startup  $I_{startup}$  current is greater than the basic current, then the startup current must be taken into consideration in the calculation. The response current for the FDE ( $I_{FDE}$ ) is calculated for each field device from the difference between the maximum current in the event of a fault and the basic current. The field device with the greatest response current is taken into consideration in the current balance sheet.

Provided that no more than one FDE responds, the following condition must be taken into consideration in the calculation of the segment current  $I_{SEG}$ :

$$\begin{aligned}
 I_{Seff.} &\geq I_{SEG} \\
 &\text{where} \\
 I_{SEG} &= \Sigma I_B + \max I_{FDE} + I_{MOD} + I_{startup}
 \end{aligned}$$

In the example the calculation formula results in the following segment current consumption  $I_{SEG}$ , where  $I_{FDE} = 0$ ,  $I_{startup} = 0$ , since the field devices used do not consume additional current in the event of a fault and the startup current is less than the bus current:

$$\begin{aligned}
 I_{SEG} &= \Sigma I_B + \max. I_{FDE} + I_{MOD} + I_{startup} \\
 &= 45 \text{ mA} + 0 \text{ mA} + 9 \text{ mA} + 0 \text{ mA} \\
 &= \underline{\underline{54 \text{ mA}}}
 \end{aligned}$$

The next step checks whether the current consumption  $I_{SEG}$  calculated is within the current limits of the fieldbus power supply. The maximum available supply current  $I_{Seff.}$  is calculated taking into consideration the current drops caused by the source impedance  $R_Q$  of the fieldbus power supply and then by the effective resistance per unit of length of the fieldbus line. Also, the condition must be met that the supply voltage at the furthest field device must be at least 9 V. To make the overall considerations easier it is assumed that all the field devices FD (refer to Fig. 8) are connected at the end of the fieldbus line.

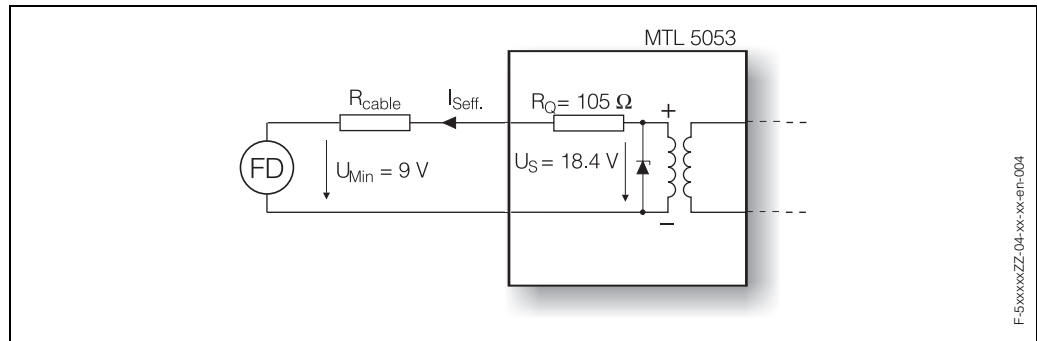


Fig. 8: Replacement circuit diagram

In order that the available supply current  $I_{Seff.}$  can be calculated the resistance value for the fieldbus line  $R_{cable}$  must first be calculated:

$$\begin{aligned}
 R_{cable} &= R_{WK} \times L_{SEG} \\
 &= 44 \Omega/\text{km} \times 0.615 \text{ km} \\
 &= \underline{\underline{27 \Omega}}
 \end{aligned}$$

Calculation of the maximum available supply current  $I_{Seff.}$  of the fieldbus power supply:

When calculating the maximum available supply current it must be ensured that a minimum supply voltage of 9 V is applied at the field devices:

$$\begin{aligned}
 I_{Seff.} &= (U_S - 9 \text{ V}) / (R_Q + R_{cable}) \\
 &= (18.4 \text{ V} - 9 \text{ V}) / (105 \Omega + 27 \Omega) \\
 &= \underline{\underline{71.2 \text{ mA}}}
 \end{aligned}$$

Observing the conditions stated, a supply current of  $I_{Seff.} = 71.2 \text{ mA}$  is available for the field devices on the bus segment. Since the actual current consumption of the segment is only 54 mA, from the point of view of the functional considerations proper functioning of the segment is ensured.

For reasons of safety the actual voltage  $U_{FG \text{ eff.}}$  of the furthest field device can be calculated as follows:

$$\begin{aligned}
 U_{FG \text{ eff.}} &= U_S - I_{SEG} \times (R_Q + R_{cable}) \\
 &= 18.4 \text{ V} - 54 \text{ mA} \times (105 \Omega + 27 \Omega) \\
 &= 18.4 \text{ V} - 7.1 \text{ V} \\
 &= \underline{\underline{11.2 \text{ V}}}
 \end{aligned}$$

Checking the conditions:

Consideration	Condition met?
$I_{seff} \geq I_{SEG}$ 71.2 mA $\geq$ 54 mA	✓ Yes
$U_{FG\ eff.} \geq 9\ V$ 11.2 V $\geq$ 9 V	✓ Yes

**Final consideration:**

From a purely functional point of view the bus segment shown in the example can be operated based on the positive results. Further optimization of the network with a view to connecting a greater number of field devices or realizing a longer line length can be achieved by selecting the right fieldbus power supply and cable type.

**Technical safety considerations**

using variant Promag 53\*\*\*-\*\*\*\*\*G

**Step 1 – compilation of technical values relevant to safety:**

*Bus power supply MTL 5053 (associated electrical apparatus)*

- Nominal values:

$U_o = 22\ V$   
 $I_o = 216\ mA$   
 $P_o = 1.2\ W$

	Explosion group		
	IIC	IIB	IIA
Capacitance $C_o$	0.165 $\mu F$	1.14 $\mu F$	4.20 $\mu F$
Inductance $L_o$	0.32 mH	3.00 mH	7.00 mH
$L/R_{ratio}$	31 $\mu H/\Omega$	126 $\mu H/\Omega$	242 $\mu H/\Omega$

Tab. 5: External connection values of bus power supply MTL 5053 depending on temperature class

*Promag 53 (explosion protected electrical apparatus with intrinsically safe FF output):*

- Nominal values:

$U_i = 30\ V$   
 $I_i = 500\ mA$   
 $P_i = 5.5\ W$   
 $L_i = 10\ \mu H$   
 $C_i = 5\ nF$

*Cerabar S (explosion protected electrical apparatus with intrinsically safe FF output):*

- Nominal values Entity:

$U_i = 24\ V$   
 $I_i = 250\ mA$   
 $P_i = 1.2\ W$   
 $L_i = 10\ \mu H$   
 $C_i = 5\ nF$

*Bus cable type 3076 from Belden (shielded bus cable):*

• Nominal values:

$$\begin{aligned}
 R' &= 24 \, \Omega/\text{km} \text{ (loop resistance)} \\
 C' &= 82 \, \text{nF}/\text{km} \text{ (capacitance per unit length between the two wires)} \\
 L' &= 623 \, \mu\text{H}/\text{km} \text{ (inductance per unit length of the two wires)} \\
 C'_{\text{LS}} &= 147 \, \text{nF}/\text{km} \text{ (capacitance per unit length wire against shielding)}
 \end{aligned}$$

*Bus termination:*

• Nominal values:

$$\begin{aligned}
 U_i &= 30 \, \text{V} \\
 P_i &= 1.2 \, \text{W} \\
 C_i &= \text{negligible}
 \end{aligned}$$

The effective capacitance of the bus line is derived first from the capacitance per unit length  $C'$ , which is effectively the capacitance between the two wires. In the case of the shielded wires the order of capacitance “wire against shielding” and “shielding against wire” must be observed. The total capacitance of the bus line is thus calculated as follows:

$$C'_{\text{eff./cable}} = (C' + 0.5 \times C'_{\text{LS}}) \times L_{\text{SEG}}$$

The total length of the bus line  $L_{\text{SEG}}$  is made up of the length of the main cable and the length of all spurs. Using the system structure illustrated in Fig. 8 the following data relevant to safety emerges for the bus line:

$$\begin{aligned}
 L_{\text{SEG}} &= L_{\text{main}} + \sum L_{\text{spurs}} \\
 &= 580 \, \text{m} \text{ (1903 ft)} + 35 \, \text{m} \text{ (115 ft)} \\
 &= \underline{\underline{615 \, \text{m} \text{ (2018 ft)}}}
 \end{aligned}$$

$$\begin{aligned}
 C'_{\text{eff./cable}} &= (C' + 0.5 \times C'_{\text{LS}}) \times L_{\text{SEG}} \\
 &= (82 \, \text{nF}/\text{km} + 0.5 \times 147 \, \text{nF}/\text{km}) \times 0.615 \, \text{km} \\
 &= \underline{\underline{95.6 \, \text{nF}}}
 \end{aligned}$$

$$\begin{aligned}
 L'_{\text{eff./cable}} &= L' \times L_{\text{SEG}} \\
 &= 623 \, \mu\text{H}/\text{km} \times 0.615 \, \text{km} \\
 &= \underline{\underline{383.1 \, \mu\text{H}}}
 \end{aligned}$$

## Step 2 – technical safety considerations

This step uses the existing data to check whether connecting the equipment is permissible from the point of view of technical safety. The conditions shown in Table 5 (Page 19) apply to these safety considerations. First the functional data of the equipment used is compared. In this consideration it is crucial that the maximum output voltage and output current of the bus power supply does not exceed the permitted maximum input voltage and input current of the individual field devices. Here we consider possible error behaviour by the bus power supply that could result in the stated maximum values on the intrinsically safe sides.

Intrinsically safe equipment	Condition	Associated equipment MTL 5053	Condition met?
<b>Promag 53</b>			
$U_i = 30 \text{ V}$	$\geq$	$U_o = 22 \text{ V}$	✓ Yes
$I_i = 500 \text{ mA}$	$\geq$	$I_o = 216 \text{ mA}$	✓ Yes
$P_i = 5.5 \text{ W}$	$\geq$	$P_o = 1.2 \text{ W}$	✓ Yes
As a further condition galvanic isolation must be provided due to the local supply			✓ Yes
<b>Cerabar S</b>			
$U_i = 24 \text{ V}$	$\geq$	$U_o = 22 \text{ V}$	✓ Yes
$I_i = 250 \text{ mA}$	$\geq$	$I_o = 216 \text{ mA}$	✓ Yes
$P_i = 1.2 \text{ W}$	$\geq$	$P_o = 1.2 \text{ W}$	✓ Yes
<b>FBT1</b>			
$U_i = 30 \text{ V}$	$\geq$	$U_o = 22 \text{ V}$	✓ Yes
$P_i = 1.2 \text{ W}$	$\geq$	$P_o = 1.2 \text{ W}$	✓ Yes

In addition to these values the limit values and the maximum permissible external capacitance  $C_o$  and inductance  $L_o$  must be observed for the supply circuit. To do this the sum of all effective inductance and capacitance in the hazardous area is formed (the internal capacitance of the bus termination is assumed to be 0). The resulting value must be less than the maximum permissible value specified by the fieldbus power supply.

The equivalent concentrated capacitance and inductance in the hazardous area is calculated as follows:

$$\begin{aligned}
 C_{\text{eff.}} &= (C_{i/\text{Promag 53}} \times 2) + (C_{i/\text{Cerabar S}} \times 2) + C'_{\text{eff./cable}} + C_{i/\text{bus termination}} \\
 &= (5 \text{ nF} \times 4) + 95.6 \text{ nF} \\
 &= 115.6 \text{ nF}
 \end{aligned}$$

$$\begin{aligned}
 L_{\text{eff.}} &= (L_{i/\text{Promag 53}} \times 2) + (L_{i/\text{Cerabar S}} \times 2) + L'_{\text{eff./cable}} \\
 &= (10 \text{ } \mu\text{H} \times 4) + 383.1 \text{ } \mu\text{H} \\
 &= 423.1 \text{ } \mu\text{H}
 \end{aligned}$$

Intrinsically safe equipment Promag 53	Condition	Associated equipment MTL 5053	Condition met?
Total capacitance $C_{\text{eff.}} = 115.6 \text{ nF}$	<	perm. capacitance for IIC $C_o = 165 \text{ nF}$	✓ Yes
Total inductance $L_{\text{eff.}} = 423.1 \text{ } \mu\text{H}$	<	perm. inductance for IIC $L_o = 320 \text{ } \mu\text{H}$	No

Tab. 6: Safety considerations (example)

If, in the example examined, the condition  $L_{\text{eff.}} < L_o$  is met, then the demonstration of intrinsic safety with respect to the electrical parameters has a positive result. In this example, however, the condition was not met since the bus line selected is too long.

Possible solutions:

1. Reduce the main line by 175 m (574 ft) to 405 m (1329 ft) (this can be achieved by installing the barrier in the immediate vicinity of Explosion Zone 1, for example).
2. Check under what conditions the manufacturer of the safety barrier or segment connector allows the use of the L/R ratio for technical safety considerations.

Since all the users are permissible for explosion group IIC and the corresponding parameters have been taken into consideration, the bus segment can be used for gases in explosion group IIC.

The permissible ambient temperature may be considered either individually for each device at the respective place of installation, or specified uniformly for the bus segment as a whole. In the latter case the lowest value of the ambient temperature applies.

Required temperature class	Intrinsically safe equipment	Maximum ambient temperature
T6	Cerabar S	104 °F
T5	Promag 53	122 °F (at 176 °F medium temperature)



### Configuration example FISCO model

Fig. 9 shows the typical structure and the associated components. The field devices are operated on a segment with the type of protection EEx ia. A galvanic isolator is used for the transition to the area with explosion risk. Field devices with a lower power consumption, such as the Cerabar S pressure gauge, are supplied via the two-wire line. In contrast, the Promag 53 as a four-wire device must be supplied via an local power supply.

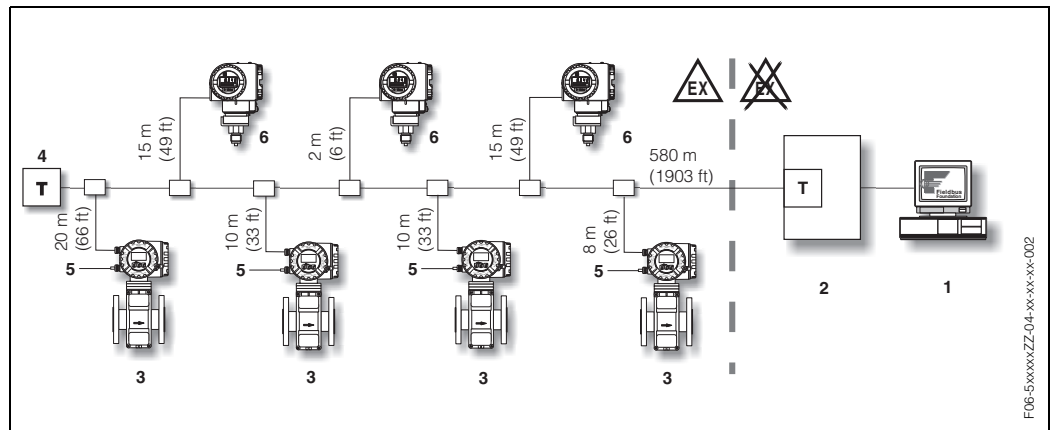


Fig. 9: Typical example of a bus connection with a fieldbus power supply Power Repeater KLD2-PR-Ex1.IEC1 (Pepperl+Fuchs)

- 1 = DCS with integrated FOUNDATION Fieldbus H1 interface card
- 2 = fieldbus power supply acc. FISCO model, Power Repeater KLD2-PR-Ex1.IEC1 (Pepperl+Fuchs)
- 3 = Promag 53 bus devices for hazardous area
- 4 = terminator (T) = bus termination
- 5 = transducer supply
- 6 = Cerabar S bus devices for hazardous area

### Functional considerations

Using the following procedure the functional considerations checks whether the desired segment structure meets the basic requirements for transmission to the physical layer in IEC 61158-2.

Step 1 – compilation of the functional characteristic values of the fieldbus components

- Fieldbus power supply according FISCO model, Power Repeater KLD2-PR-Ex1.IEC1 (Pepperl+Fuchs):
  - $U_S$  = 12.8 V (power supply voltage)
  - $I_S$  = 100 mA (power supply current)
- Fieldbus line:
  - Cable type A
  - $R_{WK}$  = 44  $\Omega$ /km (effective resistance per unit length)
- Fieldbus device Promag 53:
  - $I_B$  = 12 mA (basic current)
  - $U_B$  = 9...32 V (perm. operating voltage)
  - $I_{FDE}$  = 0 mA (fault current)
  - $I_{startup}$  = 0 (<  $I_B$ )

- Fieldbus device Cerabar S:
  - $I_B$  = 10.5 mA (basic current)
  - $U_B$  = 9...32 V (perm. operating voltage)
  - $I_{FDE}$  = 0 mA (fault current)
  - $I_{startup}$  = 0 (<  $I_B$ )

### Step 2 – calculation of cable length and checking of network structure

An approved maximum length of 1000 meters (3280 ft) has been set with the FISCO model for EEx ia IIC applications in order that the inductance and capacitance of the fieldbus cable can be ignored when used in hazardous area applications. This length comprises the length of the main cable and the total length of the drop cables together. In addition, it must be taken into account that the approved maximum length of a drop cable is 30 m (98 ft).

#### Calculation of actual cable length $L_{SEG}$ :

$$\begin{aligned}
 L_{SEG} &= L_{main} + \sum L_{spurs} \\
 &= 580 \text{ m (1903 ft)} + 80 \text{ m (262 ft)} \\
 &= \underline{\underline{660 \text{ m (2165 ft)}}}
 \end{aligned}$$

Checking the conditions:

Consideration	Condition met?
$L_{SEG} < 1000 \text{ m (3280 ft)}$ $660 \text{ m (2165 ft)} < 1000 \text{ m (3280 ft)}$	✓ Yes
$L_{spurs} < 30 \text{ m (98 ft)}$	✓ Yes

If one of the conditions is not met then the network structure must be revised.

### Step 3 – current calculation

The number of field devices that can be connected to the H1 segment depends on the fieldbus power supply selected (supply voltage and supply current) and the current consumption of the field devices. Thus, the number of devices that can be connected is reduced if a field device consumes a basic current of more than 10 mA, e.g. 20 mA. By adding up the basic currents  $I_B$  of the field devices plus the response current in the event of a fault  $I_{FDE}$  for the FDE (**F**ault **D**isconnect **E**lectronics) and the current for the data modulation  $I_{MOD}$  (+9 mA) you can determine the minimum supply current that the fieldbus power supply must supply.

If, on switching on the device, the startup  $I_{startup}$  current is greater than the basic current, then the startup current must be taken into consideration in the calculation. The response current for the FDE ( $I_{FDE}$ ) is calculated for each field device from the difference between the maximum current in the event of a fault and the basic current. The field device with the greatest response current is taken into consideration in the current balance sheet.

Provided that no more than one FDE responds, the following condition must be taken into consideration in the calculation of the segment current  $I_{SEG}$ :

$$\begin{aligned}
 I_{SEG} &\leq I_S \\
 &\text{where} \\
 I_{SEG} &= \sum I_B + \max I_{FDE} + I_{MOD} + I_{startup}
 \end{aligned}$$

In the example the calculation formula results in the following segment current consumption  $I_{SEG}$ , where  $I_{FDE} = 0$ ,  $I_{startup} = 0$ , since the field devices used do not consume additional current in the event of a fault and the startup current is less than the bus current. In addition, the modulation current  $I_{MOD}$  for the installed bus power supply KLD2-PR-Ex1.IEC1 by Pepperl+Fuchs need not be considered since the value of the supply current  $I_S$  already includes this.

$$\begin{aligned}
 I_{SEG} &= \sum I_B \\
 &= \underline{\underline{79.5 \text{ mA}}}
 \end{aligned}$$

Checking the conditions:

Consideration	Condition met?
$I_{SEG} \leq I_S$ $79.5 \text{ mA} \leq 100 \text{ mA}$	✓ Yes

*Step 4 – Voltage at the last instrument*

The cable resistance causes a segment voltage drop, which is largest at the instrument farthest away from the bus power supply. For this reason it must be ensured that the minimum operating voltage of 9 V is available at this instrument. To make the overall considerations easier it is assumed that all the field devices FD (refer to Fig. 10) are connected at the end of the fieldbus line.

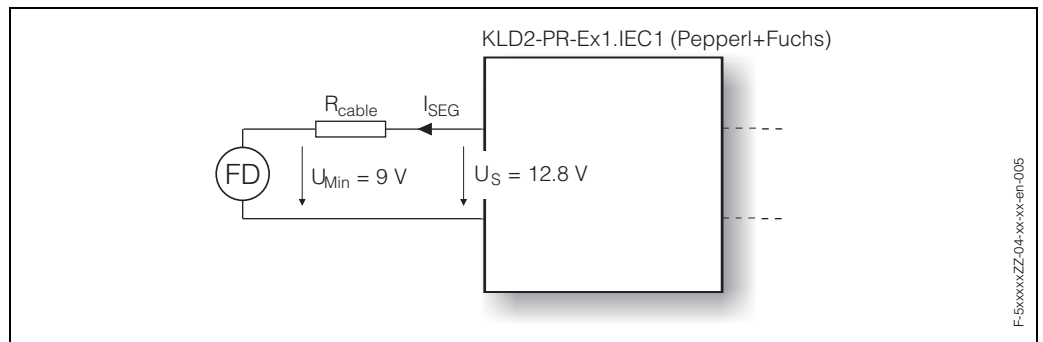


Fig. 10: Replacement circuit diagram

The resistance value  $R_{cable}$  must first be calculated in order to calculate the voltage drop caused by the fieldbus cable:

$$\begin{aligned}
 R_{cable} &= R_{WK} \times L_{SEG} \\
 &= 44 \text{ } \Omega/\text{km} \times 0.66 \text{ km} \\
 &= \underline{\underline{29 \text{ } \Omega}}
 \end{aligned}$$

Ohm's law is used to calculate the actual voltage  $U_{FG \text{ eff.}}$  at the last instrument:

$$\begin{aligned}
 U_{FG \text{ eff.}} &= U_S - (I_{SEG} \times R_{cable}) \\
 &= 12.8 \text{ V} - (79.5 \text{ mA} \times 29 \text{ } \Omega) \\
 &= 12.8 \text{ V} - 2.3 \text{ V} \\
 &= \underline{\underline{10.5 \text{ V}}}
 \end{aligned}$$

Checking the conditions:

Consideration	Condition met?
$U_{FG\text{ eff.}} \geq 9\text{ V}$	✓ Yes
$10.5\text{ V} \geq 9\text{ V}$	

**Final consideration:**

From a purely functional point of view the bus segment shown in the example can be operated based on the positive results.

**Technical safety considerations**

using variant Promag 53\*\*\*\_\*\*\*\*\*G

**Step 1 – compilation of technical values relevant to safety:**

*Fieldbus power supply (associated electrical apparatus)*

*FISCO Power Repeater KLD2-PR-Ex1.IEC1 (Pepperl+Fuchs):*

- Nominal values:

$$U_o = 15\text{ V}$$

$$I_o = 207.2\text{ mA}$$

$$P_o = 1.93\text{ W}$$

Described in the test certificate as “associated equipment”. Suitable for connection to a fieldbus system based on the FISCO model.

*Promag 53 (explosion protected electrical apparatus with intrinsically safe FF output):*

- Nominal values:

$$U_i = 30\text{ V}$$

$$I_i = 500\text{ mA}$$

$$P_i = 5.5\text{ W}$$

$$L_i = 10\text{ }\mu\text{H}$$

$$C_i = 5\text{ nF}$$

Suitable for connection to a fieldbus system based on the FISCO model.

*Cerabar S (explosion protected electrical apparatus with intrinsically safe FF output):*

- Nominal values FISCO:

$$U_i = 17.5\text{ V}$$

$$I_i = 500\text{ mA}$$

$$P_i = 5.5\text{ W}$$

$$L_i = 10\text{ }\mu\text{H}$$

$$C_i = 5\text{ nF}$$

Suitable for connection to a fieldbus system based on the FISCO model.

*Bus cable type A (shielded bus cable):*

- Nominal values:

$$R' = 24\text{ }\Omega/\text{km (loop resistance)}$$

$$C' = 82\text{ nF/km (capacitance per unit length)}$$

$$L' = 623\text{ }\mu\text{H/km (inductance per unit length)}$$

*Fieldbus connection KMD0-FT-Ex (Pepperl+Fuchs):*

• Nominal values:

$U_i$	=	24 V
$I_i$	=	280 mA
$P_i$	=	1.93 W
$R$	=	100 $\Omega$
$C$	=	1 $\mu\text{F}$

Suitable for connection to a fieldbus system based on the FISCO model.

## Step 2 – technical safety considerations acc. FISCO model

This step uses the existing data to check whether connecting the equipment is permissible from the point of view of technical safety. The conditions shown in the FISCO model apply to these safety considerations (see Page 13). First the functional data of the equipment used is compared. In this consideration it is crucial that the maximum output voltage and output current of the bus power supply does not exceed the permitted maximum input voltage and input current of the individual field devices. Here we consider possible error behaviour by the bus power supply that could result in the stated maximum values on the intrinsically safe sides.

Intrinsically safe equipment	Condition	Associated equipment FISCO Power Repeater KLD2-PR-Ex1.IEC1	Condition met?
<b>Promag 53</b>			
$U_i = 30 \text{ V}$	$\geq$	$U_o = 15 \text{ V}$	✓ Yes
$I_i = 500 \text{ mA}$	$\geq$	$I_o = 207.2 \text{ mA}$	✓ Yes
$P_i = 5.5 \text{ W}$	$\geq$	$P_o = 1.93 \text{ W}$	✓ Yes
As a further condition galvanic isolation must be provided due to the local supply			✓ Yes
<b>Cerabar S</b>			
$U_i = 17.5 \text{ V}$	$\geq$	$U_o = 15 \text{ V}$	✓ Yes
$I_i = 500 \text{ mA}$	$\geq$	$I_o = 207.2 \text{ mA}$	✓ Yes
$P_i = 5.5 \text{ W}$	$\geq$	$P_o = 1.93 \text{ W}$	✓ Yes
<b>Fieldbus connection KMD0-FT-Ex</b>			
$U_i = 24 \text{ V}$	$\geq$	$U_o = 15 \text{ V}$	✓ Yes
$I_i = 280 \text{ mA}$	$\geq$	$I_o = 207.2 \text{ mA}$	✓ Yes
$P_i = 1.93 \text{ W}$	$\geq$	$P_o = 1.93 \text{ W}$	✓ Yes

Since all the users are permissible for explosion group IIC and the corresponding parameters have been taken into consideration, the bus segment can be used for gases in explosion group IIC.

The permissible ambient temperature may be considered either individually for each device at the respective place of installation, or specified uniformly for the bus segment as a whole. In the latter case the lowest value of the ambient temperature applies.

Required temperature class	Intrinsically safe equipment	Maximum ambient temperature
T6	Cerabar S	104 °F
T5	Promag 53	122 °F (at 176 °F medium temperature)

In the next step is the verification of whether the installed bus components fulfil the conditions and limit values set in the FISCO model. This is simplified by ensuring the bus components correspond to the FISCO model. A detailed consideration of the safety-relevant nominal values is then not necessary.

Do bus components correspond to the FISCO model?	Condition met?
Power Repeater KLD2-PR-Ex1.IEC1	✓ Yes
Promag 53	✓ Yes
Cerabar S	✓ Yes
Fieldbus connection KMD0-FI-Ex	✓ Yes

The following conditions have been applied to the bus cable and network structure:

Bus cable:

Values	Condition	Limits acc. FISCO model	Condition met?
R'	> <	15 Ω/km 150 Ω/km	
C'	> <	80 nF/km 200 nF/km	
L'	> <	400 μH/km 1000 μH/km	
<b>Bus cable type A</b> R' = 24 Ω/km C' = 82 nF/km L' = 623 μH/km			✓ Yes

Network structure:

Consideration	Condition	Limits acc. FISCO model	Condition met?
Cable length including drop cables	≤	1000 m (3280 ft)	
$L_{SEG} = 660$ m (2165 ft)	≤	1000 m (3280 ft)	✓ Yes
Drop cable length	≤	30 m (98 ft)	✓ Yes

#### Final consideration:

For the example shown, intrinsic safety according to the FISCO model can be proven.

## Device identification

Promag 53 FOUNDATION Fieldbus transmitter and W/P/H sensor.

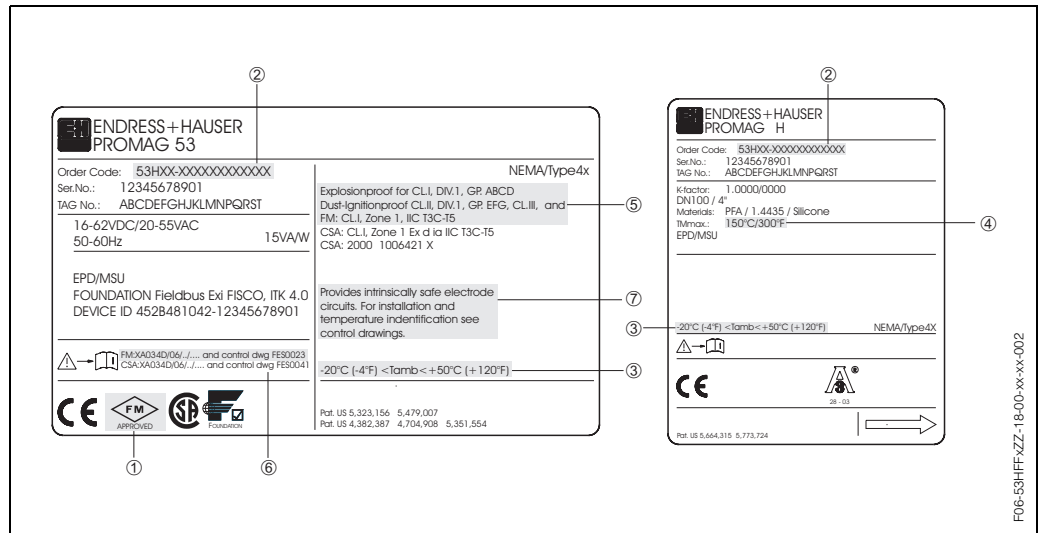


Fig. 11: Nameplate of transmitter and nameplate of sensor (example)

Key to nameplates (Figure 11)

No.	Meaning	No.	Meaning
①	Label of the notified body: Factory Mutual Research	⑤	Type of protection and explosion group for the Promag 53 FOUNDATION Fieldbus measuring system
②	Type code	⑥	Applicable Ex documentation
③	Ambient temperature range	⑦	Warning
④	Maximum medium temperature		

# Control drawings

Endress+Hauser Reinach hereby declares that the product is in conformity with the requirements of the FACTORY MUTUAL standards.

**Hazardous Locations**  
Class I Division 1 Groups ABCD or Class I Zone 1 Groups IIC and Class II and III Division 1 Groups EFG

Promag 5. W / PPromag 5. H

Keine Änderungen ohne vorherige Factory Mutual Genehmigung

**PROMAG 5. W / P / H**  
XP / I / 1 / ABCD; DIP / II, III / 1 / EFG  
AIS / I, II, III / 1 / ABCDEFG  
FM Cl. I, Zone 1, Group IIC

Temperature table

Max. ambient temperature	Max. medium temperature depending temperature classes			
	T5	T4A	T4	T3C
50 °C / 122°F	50 °C / 122°F	110 °C / 230°F		
45 °C / 113°F	50 °C / 122°F	110 °C / 230°F	130 °C / 266°F	
40 °C / 104°F	50 °C / 122°F	110 °C / 230°F	130 °C / 266°F	150 °C / 302°F

Max. allowed medium temperature depending liner material

Liner material	Max. medium temperature
PU (polyurethan)	60 °C / 140°F
HG (hard rubber)	80 °C / 176°F
PTFE	130 °C / 266°F
PFA	150 °C / 302°F

Communication Options	Control Drawing
I/O option = F,H,J	see FES 0023-0001
I/O option = G,K	see FES 0023-0002
I/O option = S,T	see FES 0023-0004

**WARNING: SUBSTITUTION OF COMPONENTS MAY IMPAIR INTRINSIC SAFETY.**

Notes:

- Control room equipment shall not use or generate more than 250 V rms.
- Caution: Use supply wires suitable for 5 °C above ambient temperature, but at least for 80 °C / 176°F.
- Class II Group G: The surface temperature of the apparatus cannot exceed 165 °C / 329°F.
- Install per NEC ANSI/NFPA 70 Article 500

Aenderungen:

A	03.12.01 / MDI	F
B		G
C		H
D		J
E		K

Ersteller: FES / ID 1006  
FILE: M:ZEICHN\FES0023\011203\_gC.DOC

**FM Control Drawing Div. 1 / Zone 1**  
Class I Zone 1

PROMAG 5x compact version

Flowtec AG, Kaegenstrasse 7, CH-4153 Reinach BL1, Postfach

Gezeichnet	3.Dez.2001	MDI
Geprüft		
Ex-geprüft	3.Dez.2001	MDI
Gesehen		

FES0023

**HAZARDOUS LOCATIONS**  
Cl. I Div. 1 Groups A,B,C,D  
Cl. I Zone 1 Group IIC  
Cl. I Div. 2 Group A,B,C,D  
Cl. I Zone 2 Group IIC  
Cl. II, III Div. 1 Group E,F,G

**NON HAZARDOUS LOCATIONS**

Notes:

**Intrinsically safe signal output:**

- Wire all intrinsically circuits per ISA RP 12.6, or in conduit per NEC ANSI/NFPA 70
- WARNING: SUBSTITUTION OF COMPONENTS MAY IMPAIR INTRINSIC SAFETY.**
- Control room equipment may not use or generate more than 250 Vrms.

**PROMAG Type: 5\*\*\*-\*\*\*\*\*G**  
**Terminals: 26, 27 (Foundation Fieldbus):**  
Intrinsically safe circuit:

$V_{max} / U_i$	$I_{max} / I_i$	$P_{max} / P_i$	$C_i$	$L_i$
30 V	500 mA	5.5 W	$\leq 5$ nF	$\leq 10$ $\mu$ H

Connect to entity approved associated apparatus with  
 $I_{sc}, I_i$  or  $I_0 \leq I_{max}$  or  $I_i$  and  
 $V_{oc}, V_i$  or  $U_0 \leq V_{max}$  or  $U_i$   
 $(P_0 \leq P_{max}$  or  $P_i)$   
 Cable parameters for Intrinsic Safety:  
 $C_{cable} \leq C_0 / C_0 - \Sigma C_i$   
 $L_{cable} \leq L_0 / L_0 - \Sigma L_i$  or  
 $L/R_{cable} \leq L/R_{Associated Apparatus}$  and  $L_i$  of each I.S. apparatus  $\leq 10$   $\mu$ H

Alternatively the intrinsically safe circuit ( Fieldbus Foundation ) can be connected according to the FISCO – Concept ( see FES 0023-0003 ).

Keine Änderungen ohne vorherige Factory Mutual Genehmigung

**Nonintrinsically safe signal output:**

- Transmitter circuit wiring in conduit in accordance with NEC ANSI/NFPA 70.
- WARNING: EXPLOSION HAZARD - SUBSTITUTION OF COMPONENTS MAY IMPAIR SUITABILITY FOR CLASS I, DIVISION 1.**
- Control room equipment may not use or generate over 250 Vrms.

PROMAG Type: 5\*\*\*-\*\*\*\*\*K  
**Terminals 26,27 (FIELDBUS FOUNDATION NON I.S.)**  
 $V \leq 32$  V,  $I = 10$  mA

Aenderungen:

A	03.12.01 / MDI	F
B		G
C		H
D		J
E		K

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Diese Zeichnung darf ohne unsere Genehmigung weder vervielfältigt werden noch dritten Personen und Konkurrenzfirmen zugänglich gemacht werden.

**FM Control Drawing Div. 1 / Zone 1**  
PROMAG 5. W / P / H  
Fieldbus Foundation I.S. installation

Flowtec AG, Kaegenstrasse 7, CH-4153 Reinach BL1, Postfach

Messstab  
%

Gezeichnet	3.Dez.2001	MDI
Geprüft		
Ex-geprüft	3.Dez.2001	MDI
Gesehen		

FES0023-0002



**FISCO CONCEPT**  
 The FISCO Concept allows interconnection of intrinsically safe apparatus to associated apparatus not specially examined in such combination. The criteria for interconnection is that the voltage (Ui or V<sub>max</sub>), the current (Ii or I<sub>max</sub>), and the power (Pi or P<sub>max</sub>) which intrinsically safe apparatus can receive and remain intrinsically safe, considering faults, must be equal or greater than the voltage (Uo, Voc or Vt), the current (Io, Isc or It) and the power (Po or P<sub>max</sub>) levels which can be delivered by the associated apparatus, considering faults and applicable factors. In addition, the maximum unprotected capacitance (Ci) and inductance (Li) of each apparatus (other than the termination) connected to the fieldbus must be less than or equal to 5 nF and 10 µH respectively.  
 In each segment only one active device, normally the associated apparatus, is allowed to provide the necessary energy for the fieldbus system. The voltage Uo (or Voc or Vt) of the associated apparatus is limited to a range of 14V to 24Vd.c. All other equipment connected to the bus cable has to be passive, meaning that they are not allowed to provide energy to the system, except a leakage current of 50µA for each connected device. Separately powered equipment needs a galvanic isolation to assure that the intrinsically safe fieldbus circuit remains passive.  
 The cable used to interconnect the devices needs to have the parameter in the following range:  
 Loop Resistance R' : 15...150 Ohm/km  
 Inductance per unit length L' : 0.4...1 mH/km  
 Capacitance per unit length C' : 80...200 nF  
 C' = C' line/line + 0.5 C' line/screen, if both lines are floating, or  
 C' = C' line/line + C' line/screen, if the screen is connected to one line  
 Length of trunk cable: ≤ 1000 m  
 Length of spur cable: ≤ 30 m  
 Length of splice: ≤ 1 m  
 At each end of the trunk cable an approved infallible line termination with following parameters is suitable:  
 R = 90...100 Ohm C = 0...2.2 µF  
 One of the allowed terminations might already be integrated in the associated apparatus. The number of passive apparatus connected to the bus segment is not limited due to I, S, reasons. If the above rules are respected, up to a total length of 1000 m (sum of trunk and all spur cables), the inductance and the capacitance of the cable will not impair the intrinsic safety of the installation.

**HAZARDOUS (CLASSIFIED) LOCATION**  
 Class I, Division 1, Groups A,B,C,D  
 Class II, Division 1, Groups E,F,G  
 Class III, Division 1

**NONHAZARDOUS LOCATION**

**PROMAG 5\* .....F/G**  
 Terminal 26 (+) Terminal 27 (-)  
 (FISCO-Model)  
 Ui (V<sub>max</sub>) = 30 V Ci ≤ 5 nF  
 Ii (I<sub>max</sub>) = 500 mA Li ≤ 10 µH  
 Pi (P<sub>max</sub>) = 5.5 W  
 Leakage current : ≤ 50µA  
 Apparatus provides galvanic isolation up to 250V rms between fieldbus circuit and any other circuit  
 Temperature Classification: T6  
 Max. ambient Temperature: 50°C / 122°F

Any FM Approved Associated Apparatus Suitable for Fisco concept

Any FM Approved Intrinsically Safe Apparatus suitable for FISCO Concept

Any FM Approved Termination with R = 90...100Ω C = 0...2.2µF

keine Änderungen ohne vorherige Factory Mutual Genehmigung

**Notes:**  
**Intrinsically safe Class I, Div. 1, Groups A,B,C,D**  
 1. Approved associated apparatus must be installed in accordance with manufacturers instructions.  
 2. FM approved associated apparatus must meet the following parameters:  
 Uo or Voc or Vt ≤ Ui (V<sub>max</sub>) and Io or Isc or It ≤ Ii (I<sub>max</sub>) and Po or P<sub>max</sub> ≤ Pi (P<sub>max</sub>)  
 3. The maximum non-hazardous area voltage must not exceed 250V  
 4. The installation must be in accordance with the National Electrical Code NFPA 70, and ANSI/ISA-Rp 12.6, (except chapter 5).  
 5. Multiple earthing of screen is allowed only, if high integrity equipotential system is realized between the points of bonding (see drawing No. FES 0014).  
 6. Caution: Use only supply wires suitable for 5°C above surrounding temperature.  
 7. Warning: Substitution of components may impair intrinsic safety.  
 8. The polarity for connection PA+ (26) and PA- (27) is of no importance due to an internal rectifier.

Änderungen:	A	03.12.01	F	Alle gesetzlichen Urheberrechte vorbehalten.	Ersetzt durch:
	B		G	Diese Zeichnung darf ohne unsere	
	C		H	Genehmigung weder vervielfältigt werden noch	Ersatz für:
	D		J	dritten Personen und Konkurrenzfirmen	Ersteller: FES / ID 1006
	E		K	zugänglich gemacht werden.	File: M:\ZEICHNUNG\FES0023\011203_sC.DOC

**FM Control Drawing Div. 1 / Zone 1**  
**PROMAG 5. W / P / H**  
**Intrinsically safe PROFIBUS PA, Fieldbus Foundation**  
**FISCO-Concept**

Massstab	Gezeichnet	3. Dez. 2001	MDI
	Geprüft		
	Ex-geprüft	3. Dez. 2001	MDI
	Gesehen		

**FES0023-0003**

Flowtec AG, Kasernenstrasse 7, CH-4153 Reinach Bl.1, Postfach

**Supplementary  
documentation**

TI 046D/06  
TI 047D/06  
TI 048D/06

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**Instruments International**

Endress+Hauser GmbH+Co.  
Weil am Rhein  
Germany  
Tel. (07621) 975-02  
Fax. (07621) 975 345



# PROline promag 53 Division 1

## Ex documentation for the BA 051D and BA 052D operating instructions

according to CANADIAN STANDARDS ASSOCIATION



Example: **Class I, Division 1, Groups ABCD**

Canadian Standards Association

Class		
I	Class I (Gas)	
II	Class II (Dust)	
III	Class III (Fibre)	

Division	
1	Division 1
2	Division 2

Group		
CSC / NEC	Gases, vapours and dusts (Examples)	Min. ignition temperature [ $\mu$ J]
A	Acetylene, carbon disulfide (Class I)	0.02
B	Hydrogen, ethyl nitrate (Class I)	0.02
C	Ethylene, isoprene (Class I)	0.06
D	Acetone, ethane, benzene (Class I)	0.18
E	Metallic powder (Class II)	
F	Coal dust (Class II)	
G	Grain dust (Class II)	
	Textile fibres (Class III)	

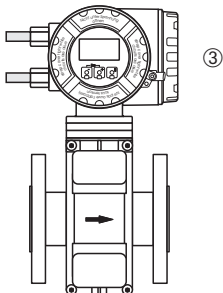
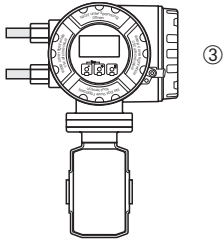
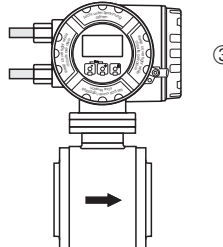
  

Type of Protection	
	Explosionproof
	Intrinsically Safe Apparatus
	Associated Apparatus with Intrinsically Safe Connections
	Nonincendive Field Wiring Circuit
	Pressurized
	Associated Pressurization Systems/Components
	Nonincendive
	Dust-Ignitionproof
	Special Protection

Temperature Class		
CSA	Maximum surface temperature	
T1	450 °C	842 °F
T2	300 °C	572 °F
T2A	280 °C	536 °F
T2B	260 °C	500 °F
T2C	230 °C	446 °F
T2D	215 °C	419 °F
T3	200 °C	392 °F
T3A	180 °C	356 °F
T3B	165 °C	329 °F
T3C	160 °C	320 °F
T4	135 °C	275 °F
T4A	120 °C	248 °F
T5	100 °C	212 °F
T6	85 °C	185 °F



Hazardous area		Safe area
Division 1 / Zone 1	Division 2 / Zone 2	
<p>Promag 53 P = DN 15...300 W = DN 25...300</p> 		
<p>Promag 53 H = DN 2...25</p> 	<p>Promag 53 H = DN 40...100</p> 	
Division 1 / Zone 1	Division 2 / Zone 2	
Hazardous area		Safe area

F06-53xxxZZ-16-xx-xx-en-001

- Promag 53 FOUNDATION Fieldbus flow measuring system in:  
Explosionproof and Dust-Ignitionproof for  
Class I, Groups ABCD or Class I, Zone 1, Group IIC  
Class II, Groups EFG  
Class III
  - For ambient and fluid temperature ranges, and temperature class, see Page 3.
- ③ Transmitter terminal compartment power supply/bus cable

## Temperature tables

### Measuring system Promag 53 (compact version)

		Max. medium temperature [°C] in					
		T5	T4A	T4	T3C	T2	T1
<i>at <math>T_a = 40\text{ °C}</math></i>							
<b>Promag H</b>	DN 2...100	50	110	130	150	150	150
<b>Promag P</b>	DN 25...200 (PFA lining)	50	110	130	150	150	150
<b>Promag P</b>	DN 15...300 (PTFE lining)	50	110	130	130	130	130
<b>Promag W</b>	DN 25...300 (polyurethan lining)	50	60	60	60	60	60
<b>Promag W</b>	DN 65...300 (hard-rubber lining)	50	80	80	80	80	80

		Max. medium temperature [°C] in					
		T5	T4A	T4	T3C	T2	T1
<i>at <math>T_a = 45\text{ °C}</math></i>							
<b>Promag H</b>	DN 2...100	50	110	130	130	130	130
<b>Promag P</b>	DN 25...200 (PFA lining)	50	110	130	130	130	130
<b>Promag P</b>	DN 15...300 (PTFE lining)	50	110	130	130	130	130
<b>Promag W</b>	DN 25...300 (polyurethan lining)	50	60	60	60	60	60
<b>Promag W</b>	DN 65...300 (hard-rubber lining)	50	80	80	80	80	80

		Max. medium temperature [°C] in					
		T5	T4A	T4	T3C	T2	T1
<i>at <math>T_a = 50\text{ °C}</math></i>							
<b>Promag H</b>	DN 2...100	50	110	110	110	110	110
<b>Promag P</b>	DN 25...200 (PFA lining)	50	110	110	110	110	110
<b>Promag P</b>	DN 15...300 (PTFE lining)	50	110	110	110	110	110
<b>Promag W</b>	DN 25...300 (polyurethan lining)	50	60	60	60	60	60
<b>Promag W</b>	DN 65...300 (hard-rubber lining)	50	80	80	80	80	80



Note:

At the specified medium temperatures, the equipment is not subjected to temperatures impermissible for the temperature class in question.



### Approvals

No. / approval type	Description
160686-1006421  (See Page 5 for notes on special conditions)	for the electric flow measuring system Promag 53 FOUNDATION Fieldbus  Identification: <b>Explosionproof and Dust-Ignitionproof for            Class I, Groups ABCD;            Class I, Zone 1, Group IIC            Class II, Groups EFG            Class III</b>

**Measuring system Promag 53 FOUNDATION Fieldbus (compact version)**

Promag 53\*\*\*.\*\*\*\*\*. [ ] | G = FOUNDATION Fieldbus, intrinsically safe  
 | K = FOUNDATION Fieldbus

Promag 53 H DN 2...100  
 Promag 53 P DN 15...600: **see description above**  
 Promag 53 W DN 25...300:

### Notified body

The Promag measuring system was tested for approval by the following named entity:

CSA: Canadian Standards Association

## Special conditions

1. Install per Canadian Electrical Code.
2. Control room equipment shall not use or generate more than 250 V rms.
3. The specified temperature class in conjunction with the ambient temperature and the medium temperature must be in compliance with the tables on Page 3.
4. Use of the devices is restricted to mediums against which the process-wetted materials are adequately resistant.
5. Use supply wires suitable for 5 °C above ambient temperature, but at least for 80 °C.
6. Devices connected to terminals Nos. 20 to 27 of the Promag 53 FOUNDATION Fieldbus transmitter must be rated for  $U_m = 260$  V and  $I_m = 500$  mA: it is impermissible to connect devices with higher ratings to these terminals.  
(Does not apply to Promag 53\*\*\*-\*\*\*\*\*G with intrinsically safe output circuit).

## General warnings



Warning:

- Installation, connection to the electricity supply, commissioning and maintenance of the devices must be carried out by qualified specialists trained to work on Ex-rated devices.
- Compliance with national regulations relating to the installation of devices in potentially explosive atmospheres is mandatory, if such regulations exist.
- Open the device only when it is de-energized (and after a delay of at least 10 minutes following shutdown of the power supply).
- The housing of the Ex-rated transmitter can be turned in 90° steps. Whereas the non-Ex version has a bayonet adapter, however, the Ex version has a thread. Recesses for centering the worm screw are provided to prevent inadvertent movement of the transmitter housing.  
It is permissible to turn the transmitter housing through a maximum of 180° during operation (in either direction), without compromising explosion protection.  
After turning the housing the worm screw must be fastened again.
- The screw cap has to be removed before the local display can be turned, and this must be done with the device de-energized (and after a delay of at least 10 minutes following shutdown of the power supply).

## Electrical connections

### Power supply connection

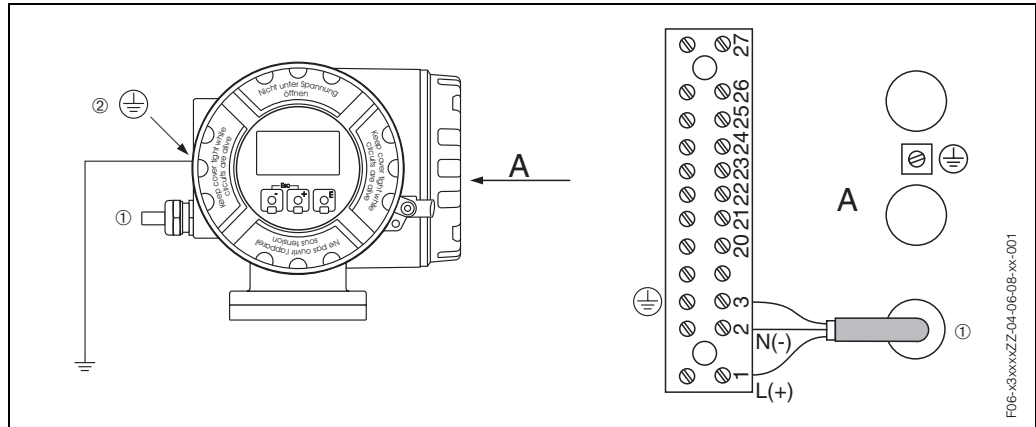


Fig. 1: ① = Power supply cable  
 ② = Ground terminal for potential equalisation  
 A = View A

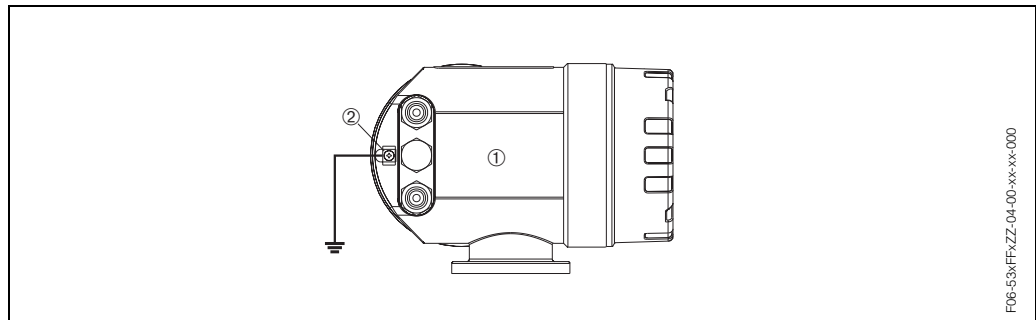


Fig. 2: Ground terminal for potential equalisation



#### Caution:

- The transmitter ① is to be securely connected to the potential equalization system using the screw terminal ② on the outside of the transmitter housing.

The table below contains the values that are identical for all versions, irrespective of the type code.

### Transmitter Promag 53

Terminals	1	2	3
	L (+)	N (-)	
Designation	Power supply ①		Protective earth
Functional values	AC: U = 85...260 V or AC: U = 20...55 V or DC: U = 16...62 V  Power consumption: 15 VA / 15 W		Caution: Follow ground network requirements for the facility
Intrinsically safe circuit	no		
U <sub>max</sub> =	260 V AC		



**Input/output circuit**

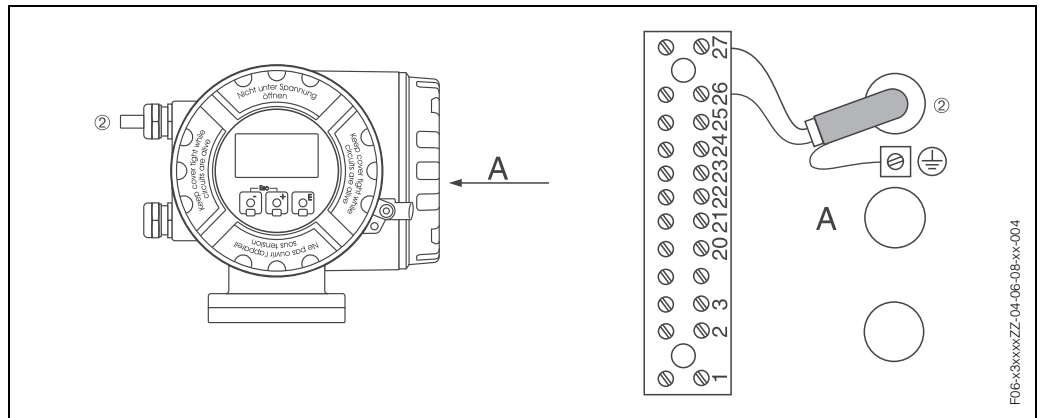


Fig. 3: ② = Bus cable (FOUNDATION Fieldbus)  
A = View A



**Note:**

The table below contains the values that are not identical for all versions, in other words which depend on the type code (type of device). Always remember to compare the type code in the table with the code on the nameplate of your device.

**Transmitter Promag 53\*\*\*-\*\*\*\*\*G**

Terminals	20	21	22	23	24	25	26	27
	+	-	+	-	+	-	+	-
Designation							FOUNDATION Fieldbus ②	
Functional values							$U_B = 9...32 \text{ V DC}$ $I_B = 12 \text{ mA}$	
Intrinsically safe circuit							EEx ia	
$U_i =$							30 V DC	
$I_i =$							500 mA	
$P_i =$							5.5 W	
$L_i =$							10 $\mu\text{H}$	
$C_i =$							5 nF	

**Transmitter Promag 53\*\*\*-\*\*\*\*\*K**

Terminals	20	21	22	23	24	25	26	27
	+	-	+	-	+	-	+	-
Designation							FOUNDATION Fieldbus ②	
Functional values							$U_B = 9...32 \text{ V DC}$ $I_B = 12 \text{ mA}$	
Intrinsically safe circuit							no	
$U_{\text{max}} =$							260 V AC	
$I_{\text{max}} =$							500 mA	

## Service adapter

The service adapter is exclusively for connection to E+H approved service interfaces.



Warning:

It is not permissible to connect the service adapter in explosive atmospheres.

## Device fuse



Warning:

Use only fuses of the following types; the fuses are installed on the power supply board:

- Voltage 20...55 V AC / 16...62 V DC:  
fuse 2.0 A slow-blow, disconnect capacity 1500 A  
(Schurter, 0001.2503 or Wickmann, Standard Type 181 2.0 A)
- Voltage 85...260 V AC:  
fuse 0.8 A slow-blow, disconnect capacity 1500 A  
(Schurter, 0001.2507 or Wickmann, Standard Type 181 0.8 A)

## Cable entries

For number reference see the figure on Page 2.

- ③ *Cable entries for the transmitter terminal compartment power supply / bus cable: (Promag 53\*\*\*-\*\*\*\*N\*\*\*\*\*)*  
Thread for cable entries 1/2" NPT.

Make sure that the cable entries are secured to prevent them from working loose.

## Technical data

### Dimensions wall-mount housing

Weight approx. 6.7 kg

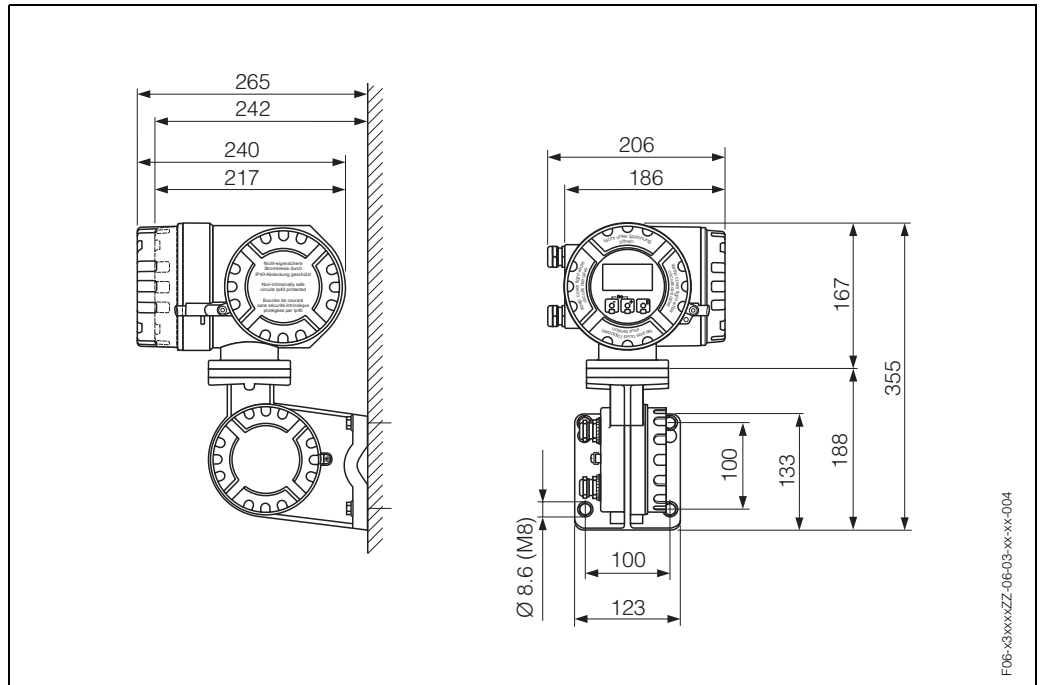


Fig. 4: Dimensions wall-mount housing

F06-X3xxxZZ-06-03-xx-xx-004

## Bus cable for FOUNDATION Fieldbus

The Fieldbus FOUNDATION defines four different types of cable in the specification creating the physical transmission layer (FF-816) which is analogous to IEC 61158-2. A two-core cable is always specified.

The electrical data has not been specified but determines important characteristics of the design of the fieldbus, such as distances bridged, number of participants, electro-magnetic compatibility, etc.

Two of the four cable types in the standard are specified in the following table.

	<b>Cable type A (reference)</b>	<b>Cable type B</b>
<i>Cable construction</i>	twisted pair, shielded	one or more twisted pairs, fully shielded
<i>Core cross-section (nominal)</i>	0.8 mm <sup>2</sup> (AWG 18)	0.32 mm <sup>2</sup> (AWG 22)
<i>Loop resistance (direct current)</i>	44 Ω/km	112 Ω/km
<i>Impedance at 31.25 kHz</i>	100 Ω ± 20%	100 Ω ± 30%
<i>Attenuation constant at 39 kHz</i>	3 dB/km	5 dB/km
<i>Capacitive unsymmetry</i>	2 nF/km	2 nF/km
<i>Envelope delay distortion (7.9...39 kHz)</i>	1.7 μs/km	**
<i>Degree of voltage of shielding</i>	90%	**
<i>Max. bus segment length (inc. spur lines)</i>	1900 m	1200 m

Tab. 1: Cable types

We recommend the use of cables meeting the minimum requirements of type A as transmission medium, particularly for the installation of new systems. The recommended network expansion is made up of the length of the main cable and the length of all spurs. The line between distribution box and field device is described as a spur. The maximum length of a spur depends on the number of spurs (>1 m). A maximum of four field devices can be connected to a spur.

<b>Number of spurs</b>	<b>1...12</b>	<b>13...14</b>	<b>15...18</b>	<b>19...24</b>	<b>25...32</b>
Max. length per spur	120 m	90 m	60 m	30 m	1 m

Tab. 2: Table of possible spur line lengths

The following table shows examples of FOUNDATION Fieldbus bus cables (type A) from various manufacturers.

<b>Supplier</b>	<b>Model</b>	<b>Order number</b>
Belden	3076	–
Kerpen	FB-02YS (St+C) Y-FL	74220001 (light blue) 74220004 (black)
Siemens	SIMATIC NET bus cable	6XV1830-5AH10 (light blue) 6XV1830-5BH10 (black)

Tab. 3: Possible cable suppliers

**Bus termination**

The start and end of each fieldbus segment are always to be terminated with a bus terminator.

- In the case of a branched bus segment the measuring device furthest from the segment connector represents the end of the bus.
- If the fieldbus is extended with a repeater then the extension must also be terminated at both ends.

**Selecting and connecting components**

The FOUNDATION Fieldbus allows several devices from different manufacturers to be generally connected to a bus segment. When selecting components for use in areas with an explosion risk only components marked as intrinsically safe, explosion-protected electrical equipment or as intrinsically safe associated electrical equipment may be used. When combining different fieldbus devices and fieldbus components, in addition to functional considerations, technical safety factors must be considered if explosion protection is to be ensured.

**Implementation of intrinsic safety in the FOUNDATION Fieldbus H1**

The FOUNDATION Fieldbus H1 can be made intrinsically safe for use in areas with an explosion risk (EEx i). To do this, according to the FOUNDATION Fieldbus specification a suitable safety component must be installed (FF-816) between the safe area and the area with an explosion risk. The intrinsically safe bus segment can be supplied either by a non-intrinsically safe power supply with a safety barrier downstream or by a fieldbus power supply with an intrinsically safe output.

It is recommended that the cable shielding be grounded at both ends (refer to Fig. 6, Page 14).

Installation example of a galvanic isolator with bus feed:

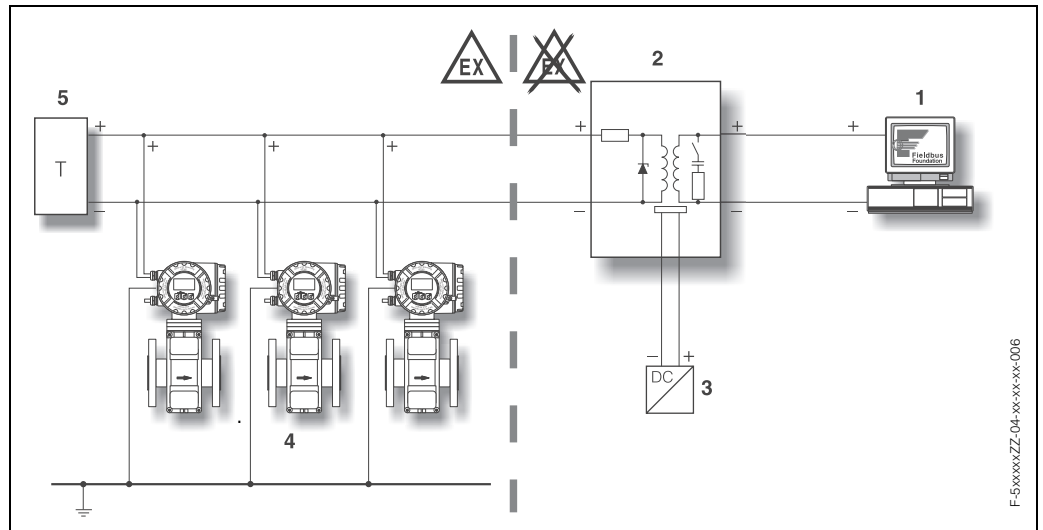


Fig. 5: Typical embodiment of a galvanic isolator including fieldbus power supply

- 1 = DCS with integrated FOUNDATION Fieldbus H1 interface card
- 2 = fieldbus power supply: galvanic isolator
- 3 = fieldbus power supply
- 4 = Promag 53 bus devices for hazardous area
- 5 = terminator (T) = bus termination

## Proof of intrinsic safety

Proof of intrinsic safety for the intrinsically safe bus segment can be made by using one of the following models:

- Entity model
- FISCO model

Both models differ from one another by their consideration of the cable. While the FISCO model considers the transmission line as distributed inductance and capacitance, the basis of this consideration for the Entity model is concentrated inductance and capacitance. The result of this is that lower quantities of power can be transmitted with the Entity model into the Ex area, and that the number of field devices that can be operated on a power repeater is therefore lower than with the FISCO model.

In the case of failure, instruments from different manufacturers can be exchanged when their safety-relevant data is taken into consideration. This data is: electrical parameters, device group and category, and the temperature class.

Both these models are briefly described in the following.

### The Entity model

The Entity model is based on the observation that the cable represents concentrated inductance and capacitance. The result is that less electrical power can be transmitted into the area subject to the risk of explosion when compared with the FISCO model.

The following conditions must be met in the safety according to the entity model considerations:

Field device Hazardous area	Mandatory	Power supply Safe area
Maximum voltage [U <sub>i</sub> ]	≥	Idle voltage of the safety element [U <sub>o</sub> ]
Maximum current [I <sub>i</sub> ]	≥	Short-circuit current [I <sub>o</sub> ]
Maximum power [P <sub>i</sub> ]	≥	[P <sub>o</sub> ]
Effective internal capacitance [C <sub>i</sub> ] + cable capacitance	≤	Maximum permitted external capacitance [C <sub>o</sub> ]
Effective internal inductance [L <sub>i</sub> ] + cable inductance	≤	Maximum permitted external inductance [L <sub>o</sub> ]

Tab. 4: General dependencies

In addition, the following measures must be taken:

- determine permissible explosion group for the bus segment
- determine all effective energy stores (L<sub>i</sub>, C<sub>i</sub>, capacitance and inductance per unit length)
- check locally supplied operating units for galvanic isolation
- harmonize temperature class and ambient temperature



Note:  
Configuration example see Page 16

## The FISCO model

The German Federal Physical-Technical Institute (PTB) has developed the FISCO model which was published in Report PTB-W-53 "Examination on Intrinsic Safety for Field Bus Systems".

The FISCO model makes possible the interconnection of intrinsically safe apparatus and one intrinsically safe associated apparatus, without having to have separate certification for respective connections.

The criteria for the intrinsic safety of an interconnection (bus segment) is given under the following interrelationships:

1. To transmit power and data, the bus system uses the physical configuration defined by IEC 61158-2. This is the case for FOUNDATION Fieldbus and the H1 bus.
2. Only one active source is permitted on a bus segment (here the power repeater). All other components work as passive current sinks.
3. The basic current consumption of a field device is at least 10 mA.
4.  $U_i$ ,  $I_i$  and  $P_i$  of the bus device  $\geq U_o$ ,  $I_o$  and  $P_o$  of the associated equipment (bus power supply).
5. Each instrument must fulfill the following requirement:  $C_i \leq 5$  nF,  $L_i \leq 10$   $\mu$ H
6. The permissible line length for EEx ia IIC applications is 1000 m.
7. The permissible spur length for Ex applications is 30 m per spur.
8. The transmission line that is used must conform to the following cable parameters:  
Resistor coating:  $15 \Omega/\text{km} < R' < 150 \Omega/\text{km}$   
Inductance coating:  $0.4 \text{ mH}/\text{km} < L' < 1 \text{ mH}/\text{km}$   
Capacitance coating:  $80 \text{ nF}/\text{km} < C' < 200 \text{ nF}/\text{km}$  (including the shield)
9. The bus segment must be terminated on both ends of the line with a terminal bus resistor. A terminal resistor is integrated into the power repeater so that an external bus terminator is only required on the other end. According to the FISCO model the fieldbus terminator must conform to the following limits:  
–  $90 \Omega < R < 100 \Omega$   
–  $0 \mu\text{F} < C < 2.2 \mu\text{F}$



Note:  
Configuration example see Page 23

## Potential equalisation with shielding grounded at both ends

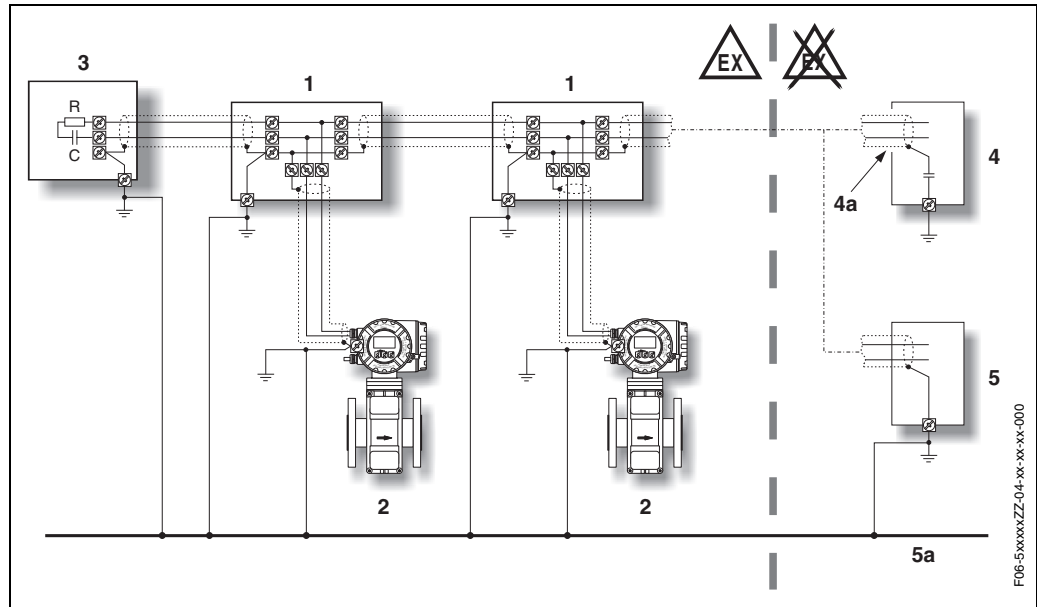


Fig. 6: Examples of the connection of potential equalisation lines

- 1 = distributor/T-box
- 2 = Promag 53 bus devices for hazardous area
- 3 = bus termination:  $R = 90 \dots 100 \Omega$ ,  $C = 0 \dots 2.2 \mu F$
- 4 = fieldbus power supply variant 4a
- 4a = shielding connected via capacitor
- 5 = fieldbus power supply variant 5a
- 5a = potential equalisation line led out

### Variant 4/4a:

With capacitive grounding of the shielding in the safe area the potential equalisation line does not need to be led out of the safe area.

Use small capacitors (e.g. 1 nF, 1500 V, dielectric strength, ceramic). The total capacitance connected at the shielding must not exceed 10 nF.

### Variant 5/5a:

Potential equalisation line is led out of the safe area.



## Network configuration for FOUNDATION Fieldbus H1

### General remarks

Various aspects are to be considered when configuring a FOUNDATION Fieldbus H1 segment and these must essentially be checked by two general types of considerations:

### Functional considerations

In the functional considerations, the characteristic of the technical function data laid down in IEC 61158-2 for the transmission technology of the FOUNDATION Fieldbus H1 and the physical network structure is checked. Here it must always be ensured that the total base currents of all bus participants does not exceed the maximum permissible feed current of the bus power supply and that the field devices are always supplied with a minimum bus voltage of 9 V.

### Technical safety considerations

For use of the FOUNDATION Fieldbus H1 in an area with an explosion risk, proof of intrinsic safety is to be provided for the entire bus segment by means of the technical safety considerations. Proof of intrinsic safety for the intrinsically safe bus segment can be made by using one of the following models:

#### *Entity model*

The safety considerations correspond to those in a conventional 4...20 mA measuring circuit. The only exception is that here more than one field device is supplied by the power supply. The safety considerations must result in the knowledge that the fieldbus power supply does not exceed the safety parameters ( $P$ -,  $U$ -,  $I$ -values) of the field devices and that the inductance and capacitance are within the permissible limits (example see Page 16).

#### *FISCO model*

If proof of intrinsic safety is made according to the FISCO model, it is to be verified that all components connected to the bus segment (field instruments, bus power supplies, bus terminator) are laid out according to the FISCO model. If this is the case, it must be proven that for each bus component the values of  $U_i$ ,  $I_i$  and  $P_i$  are greater or the same as the values of  $U_o$ ,  $I_o$  and  $P_o$  for the associated equipment (bus power supply). Example see Page 23.

### Configuration example for a FOUNDATION Fieldbus H1 segment

Based on the following example, the functional and safety-relevant considerations and calculations for the specification of a FOUNDATION Fieldbus H1 segment are carried out.

## Configuration example Entity model

Fig. 7 shows the typical structure and the associated components. The field devices are operated on a segment with the type of protection EEx ia. A galvanic isolator is used for the transition to the area with explosion risk. Field devices with a lower power consumption, such as the Cerabar S pressure gauge, are supplied via the two-wire line. In contrast, the Promag 53 as a four-wire device must be supplied via an local power supply.

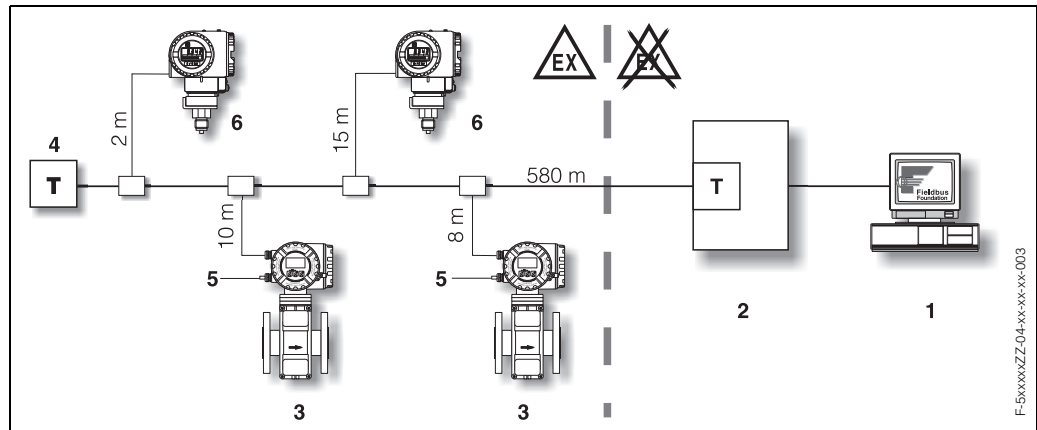


Fig. 7: Typical example of a bus connection with a fieldbus power supply of type MTL 5053

- 1 = DCS with integrated FOUNDATION Fieldbus H1 interface card
- 2 = fieldbus power supply, model MTL 5053
- 3 = Promag 53 bus devices for hazardous area
- 4 = terminator (T) = bus termination
- 5 = transducer supply
- 6 = Cerabar S bus devices for hazardous area

### Functional considerations

Using the following procedure the functional considerations checks whether the desired segment structure meets the basic requirements for transmission to the physical layer in IEC 61158-2.

*Step 1 – compilation of the functional characteristic values of the fieldbus components*

- Fieldbus power supply MTL 5053:

$$\begin{aligned}
 U_S &= 18.4 \text{ V} \\
 I_S &= 80 \text{ mA} \\
 R_Q &= 105 \Omega \text{ (source impedance)}
 \end{aligned}$$

- Fieldbus line:

Cable type A

$$\begin{aligned}
 R_{WK} &= 44 \Omega/\text{km} \text{ (effective resistance per unit length)} \\
 \text{max. permissible cable length } L_{\text{perm.}} &= 1900 \text{ m}
 \end{aligned}$$

- Fieldbus device Promag 53:

$$\begin{aligned}
 I_B &= 12 \text{ mA (basic current)} \\
 U_B &= 9...32 \text{ V (perm. operating voltage)} \\
 I_{FDE} &= 0 \text{ mA (fault current)} \\
 I_{\text{startup}} &= 0 (< I_B)
 \end{aligned}$$

- Fieldbus device Cerabar S:

$$\begin{aligned}
 I_B &= 10.5 \text{ mA (basic current)} \\
 U_B &= 9...32 \text{ V (perm. operating voltage)} \\
 I_{FDE} &= 0 \text{ mA (fault current)} \\
 I_{\text{startup}} &= 0 (< I_B)
 \end{aligned}$$

### Step 2 – calculation of cable length and checking of network structure

The maximum cable length is always determined by the type of cable used. The actual cable length, which is made up of the length of the main cable and the length of the spur lines, must not exceed this value. The spur lines are also to be checked (refer to Table 2, Page 10). The following restrictions apply to the specification of the cable length and network structure:

- Where cable type A is used the cable length  $L_{perm.}$  may be max. 1900 m.
- Checking the spur line lengths (refer to Table 2, Page 10).

Calculation of actual cable length:

$$\begin{aligned}
 L_{SEG} &= L_{main.} + \Sigma L_{spurs} \\
 &= 580 \text{ m} + 35 \text{ m} \\
 &= \underline{\underline{615 \text{ m}}}
 \end{aligned}$$

Checking the conditions

Consideration	Condition met?
$L_{SEG} < L_{perm.}$	✓ Yes
$L_{spurs} < 120 \text{ m}$	✓ Yes

If one of the conditions is not met then the network structure must be revised.

### Step 3 – current calculation

The number of field devices that can be connected to the H1 segment depends on the fieldbus power supply selected (supply voltage and supply current) and the current consumption of the field devices. Thus, the number of devices that can be connected is reduced if a field device consumes a basic current of more than 10 mA, e.g. 20 mA. By adding up the basic currents  $I_B$  of the field devices plus the response current in the event of a fault  $I_{FDE}$  for the FDE (**F**ault **D**isconnect **E**lectronics) and the current for the data modulation  $I_{MOD}$  (+9 mA) you can determine the minimum supply current that the fieldbus power supply must supply.

If, on switching on the device, the startup  $I_{startup}$  current is greater than the basic current, then the startup current must be taken into consideration in the calculation. The response current for the FDE ( $I_{FDE}$ ) is calculated for each field device from the difference between the maximum current in the event of a fault and the basic current. The field device with the greatest response current is taken into consideration in the current balance sheet.

Provided that no more than one FDE responds, the following condition must be taken into consideration in the calculation of the segment current  $I_{SEG}$ :

$$\begin{aligned}
 I_{Seff.} &\geq I_{SEG} \\
 &\text{where} \\
 I_{SEG} &= \Sigma I_B + \max I_{FDE} + I_{MOD} + I_{startup}
 \end{aligned}$$

In the example the calculation formula results in the following segment current consumption  $I_{SEG}$ , where  $I_{FDE} = 0$ ,  $I_{startup} = 0$ , since the field devices used do not consume additional current in the event of a fault and the startup current is less than the bus current:

$$\begin{aligned}
 I_{SEG} &= \Sigma I_B + \max. I_{FDE} + I_{MOD} + I_{startup} \\
 &= 45 \text{ mA} + 0 \text{ mA} + 9 \text{ mA} + 0 \text{ mA} \\
 &= \underline{\underline{54 \text{ mA}}}
 \end{aligned}$$

The next step checks whether the current consumption  $I_{SEG}$  calculated is within the current limits of the fieldbus power supply. The maximum available supply current  $I_{Seff.}$  is calculated taking into consideration the current drops caused by the source impedance  $R_Q$  of the fieldbus power supply and then by the effective resistance per unit of length of the fieldbus line. Also, the condition must be met that the supply voltage at the furthest field device must be at least 9 V. To make the overall considerations easier it is assumed that all the field devices FD (refer to Fig. 8) are connected at the end of the fieldbus line.

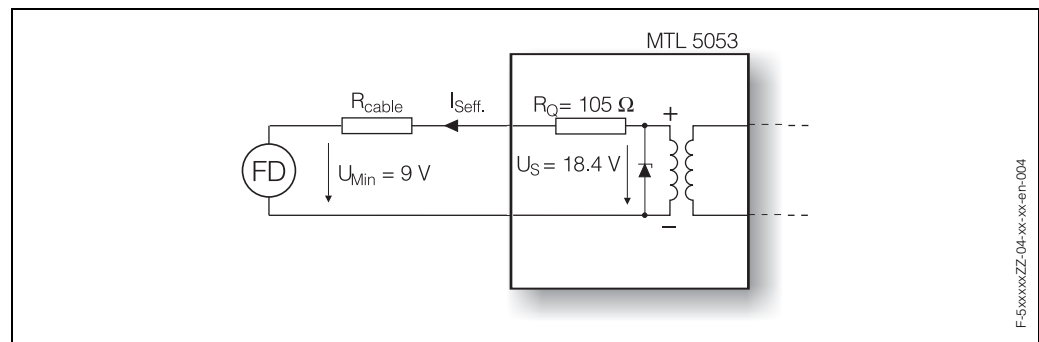


Fig. 8: Replacement circuit diagram

In order that the available supply current  $I_{Seff.}$  can be calculated the resistance value for the fieldbus line  $R_{cable}$  must first be calculated:

$$\begin{aligned}
 R_{cable} &= R_{WK} \times L_{SEG} \\
 &= 44 \Omega/\text{km} \times 0.615 \text{ km} \\
 &= \underline{\underline{27 \Omega}}
 \end{aligned}$$

Calculation of the maximum available supply current  $I_{Seff.}$  of the fieldbus power supply:

When calculating the maximum available supply current it must be ensured that a minimum supply voltage of 9 V is applied at the field devices:

$$\begin{aligned}
 I_{Seff.} &= (U_S - 9 \text{ V}) / (R_Q + R_{cable}) \\
 &= (18.4 \text{ V} - 9 \text{ V}) / (105 \Omega + 27 \Omega) \\
 &= \underline{\underline{71.2 \text{ mA}}}
 \end{aligned}$$

Observing the conditions stated, a supply current of  $I_{Seff.} = 71.2 \text{ mA}$  is available for the field devices on the bus segment. Since the actual current consumption of the segment is only 54 mA, from the point of view of the functional considerations proper functioning of the segment is ensured.

For reasons of safety the actual voltage  $U_{FG \text{ eff.}}$  of the furthest field device can be calculated as follows:

$$\begin{aligned}
 U_{FG \text{ eff.}} &= U_S - I_{SEG} \times (R_Q + R_{cable}) \\
 &= 18.4 \text{ V} - 54 \text{ mA} \times (105 \Omega + 27 \Omega) \\
 &= 18.4 \text{ V} - 7.1 \text{ V} \\
 &= \underline{\underline{11.2 \text{ V}}}
 \end{aligned}$$

Checking the conditions:

Consideration	Condition met?
$I_{seff} \geq I_{SEG}$ 71.2 mA $\geq$ 54 mA	✓ Yes
$U_{FG\ eff.} \geq 9\ V$ 11.2 V $\geq$ 9 V	✓ Yes

**Final consideration:**

From a purely functional point of view the bus segment shown in the example can be operated based on the positive results. Further optimization of the network with a view to connecting a greater number of field devices or realizing a longer line length can be achieved by selecting the right fieldbus power supply and cable type.

**Technical safety considerations**

using variant Promag 53\*\*\*-\*\*\*\*\*G

**Step 1 – compilation of technical values relevant to safety:**

*Bus power supply MTL 5053 (associated electrical apparatus)*

- Nominal values:

$U_o = 22\ V$   
 $I_o = 216\ mA$   
 $P_o = 1.2\ W$

	Explosion group		
	IIC	IIB	IIA
Capacitance $C_o$	0.165 $\mu F$	1.14 $\mu F$	4.20 $\mu F$
Inductance $L_o$	0.32 mH	3.00 mH	7.00 mH
$L/R_{ratio}$	31 $\mu H/\Omega$	126 $\mu H/\Omega$	242 $\mu H/\Omega$

Tab. 5: External connection values of bus power supply MTL 5053 depending on temperature class

*Promag 53 (explosion protected electrical apparatus with intrinsically safe FF output):*

- Nominal values:

$U_i = 30\ V$   
 $I_i = 500\ mA$   
 $P_i = 5.5\ W$   
 $L_i = 10\ \mu H$   
 $C_i = 5\ nF$

*Cerabar S (explosion protected electrical apparatus with intrinsically safe FF output):*

- Nominal values Entity:

$U_i = 24\ V$   
 $I_i = 250\ mA$   
 $P_i = 1.2\ W$   
 $L_i = 10\ \mu H$   
 $C_i = 5\ nF$

*Bus cable type 3076 from Belden (shielded bus cable):*

• Nominal values:

$$\begin{aligned}
 R' &= 24 \text{ } \Omega/\text{km} \text{ (loop resistance)} \\
 C' &= 82 \text{ nF/km (capacitance per unit length between the two wires)} \\
 L' &= 623 \text{ } \mu\text{H/km (inductance per unit length of the two wires)} \\
 C'_{LS} &= 147 \text{ nF/km (capacitance per unit length wire against shielding)}
 \end{aligned}$$

*Bus termination:*

• Nominal values:

$$\begin{aligned}
 U_i &= 30 \text{ V} \\
 P_i &= 1.2 \text{ W} \\
 C_i &= \text{negligible}
 \end{aligned}$$

The effective capacitance of the bus line is derived first from the capacitance per unit length  $C'$ , which is effectively the capacitance between the two wires. In the case of the shielded wires the order of capacitance “wire against shielding” and “shielding against wire” must be observed. The total capacitance of the bus line is thus calculated as follows:

$$C'_{\text{eff./cable}} = (C' + 0.5 \times C'_{LS}) \times L_{\text{SEG}}$$

The total length of the bus line  $L_{\text{SEG}}$  is made up of the length of the main cable and the length of all spurs. Using the system structure illustrated in Fig. 8 the following data relevant to safety emerges for the bus line:

$$\begin{aligned}
 L_{\text{SEG}} &= L_{\text{main}} + \sum L_{\text{spurs}} \\
 &= 580 \text{ m} + 35 \text{ m} \\
 &= \underline{\underline{615 \text{ m}}}
 \end{aligned}$$

$$\begin{aligned}
 C'_{\text{eff./cable}} &= (C' + 0.5 \times C'_{LS}) \times L_{\text{SEG}} \\
 &= (82 \text{ nF/km} + 0.5 \times 147 \text{ nF/km}) \times 0.615 \text{ km} \\
 &= \underline{\underline{95.6 \text{ nF}}}
 \end{aligned}$$

$$\begin{aligned}
 L'_{\text{eff./cable}} &= L' \times L_{\text{SEG}} \\
 &= 623 \text{ } \mu\text{H/km} \times 0.615 \text{ km} \\
 &= \underline{\underline{383.1 \text{ } \mu\text{H}}}
 \end{aligned}$$

## Step 2 – technical safety considerations

This step uses the existing data to check whether connecting the equipment is permissible from the point of view of technical safety. The conditions shown in Table 5 (Page 19) apply to these safety considerations. First the functional data of the equipment used is compared. In this consideration it is crucial that the maximum output voltage and output current of the bus power supply does not exceed the permitted maximum input voltage and input current of the individual field devices. Here we consider possible error behaviour by the bus power supply that could result in the stated maximum values on the intrinsically safe sides.

Intrinsically safe equipment	Condition	Associated equipment MTL 5053	Condition met?
<b>Promag 53</b>			
$U_i = 30 \text{ V}$	$\geq$	$U_o = 22 \text{ V}$	✓ Yes
$I_i = 500 \text{ mA}$	$\geq$	$I_o = 216 \text{ mA}$	✓ Yes
$P_i = 5.5 \text{ W}$	$\geq$	$P_o = 1.2 \text{ W}$	✓ Yes
As a further condition galvanic isolation must be provided due to the local supply			✓ Yes
<b>Cerabar S</b>			
$U_i = 24 \text{ V}$	$\geq$	$U_o = 22 \text{ V}$	✓ Yes
$I_i = 250 \text{ mA}$	$\geq$	$I_o = 216 \text{ mA}$	✓ Yes
$P_i = 1.2 \text{ W}$	$\geq$	$P_o = 1.2 \text{ W}$	✓ Yes
<b>FBT1</b>			
$U_i = 30 \text{ V}$	$\geq$	$U_o = 22 \text{ V}$	✓ Yes
$P_i = 1.2 \text{ W}$	$\geq$	$P_o = 1.2 \text{ W}$	✓ Yes

In addition to these values the limit values and the maximum permissible external capacitance  $C_o$  and inductance  $L_o$  must be observed for the supply circuit. To do this the sum of all effective inductance and capacitance in the hazardous area is formed (the internal capacitance of the bus termination is assumed to be 0). The resulting value must be less than the maximum permissible value specified by the fieldbus power supply.

The equivalent concentrated capacitance and inductance in the hazardous area is calculated as follows:

$$\begin{aligned}
 C_{\text{eff.}} &= (C_{i/\text{Promag 53}} \times 2) + (C_{i/\text{Cerabar S}} \times 2) + C'_{\text{eff./cable}} + C_{i/\text{bus termination}} \\
 &= (5 \text{ nF} \times 4) + 95.6 \text{ nF} \\
 &= 115.6 \text{ nF}
 \end{aligned}$$

$$\begin{aligned}
 L_{\text{eff.}} &= (L_{i/\text{Promag 53}} \times 2) + (L_{i/\text{Cerabar S}} \times 2) + L'_{\text{eff./cable}} \\
 &= (10 \text{ } \mu\text{H} \times 4) + 383.1 \text{ } \mu\text{H} \\
 &= 423.1 \text{ } \mu\text{H}
 \end{aligned}$$

Intrinsically safe equipment Promag 53	Condition	Associated equipment MTL 5053	Condition met?
Total capacitance $C_{\text{eff.}} = 115.6 \text{ nF}$	<	perm. capacitance for IIC $C_o = 165 \text{ nF}$	✓ Yes
Total inductance $L_{\text{eff.}} = 423.1 \text{ } \mu\text{H}$	<	perm. inductance for IIC $L_o = 320 \text{ } \mu\text{H}$	No

Tab. 6: Safety considerations (example)

If, in the example examined, the condition  $L_{\text{eff.}} < L_o$  is met, then the demonstration of intrinsic safety with respect to the electrical parameters has a positive result. In this example, however, the condition was not met since the bus line selected is too long.

Possible solutions:

1. Reduce the main line by 175 m to 405 m (this can be achieved by installing the barrier in the immediate vicinity of Explosion Zone 1, for example).
2. Check under what conditions the manufacturer of the safety barrier or segment connector allows the use of the L/R ratio for technical safety considerations.

Since all the users are permissible for explosion group IIC and the corresponding parameters have been taken into consideration, the bus segment can be used for gases in explosion group IIC.

The permissible ambient temperature may be considered either individually for each device at the respective place of installation, or specified uniformly for the bus segment as a whole. In the latter case the lowest value of the ambient temperature applies.

Required temperature class	Intrinsically safe equipment	Maximum ambient temperature
T6	Cerabar S	40 °C
T5	Promag 53	50 °C (at 80 °C medium temperature)



## Configuration example FISCO model

Fig. 9 shows the typical structure and the associated components. The field devices are operated on a segment with the type of protection EEx ia. A galvanic isolator is used for the transition to the area with explosion risk. Field devices with a lower power consumption, such as the Cerabar S pressure gauge, are supplied via the two-wire line. In contrast, the Promag 53 as a four-wire device must be supplied via an local power supply.

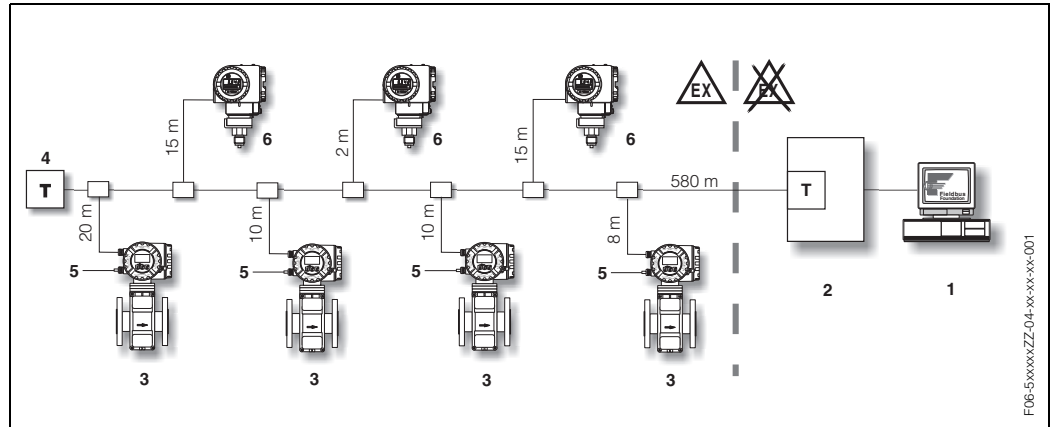


Fig. 9: Typical example of a bus connection with a fieldbus power supply  
Power Repeater KLD2-PR-Ex1.IEC1 (Pepperl+Fuchs)

- 1 = DCS with integrated FOUNDATION Fieldbus H1 interface card  
 2 = fieldbus power supply acc. FISCO model, Power Repeater KLD2-PR-Ex1.IEC1 (Pepperl+Fuchs)  
 3 = Promag 53 bus devices for hazardous area  
 4 = terminator (T) = bus termination  
 5 = transducer supply  
 6 = Cerabar S bus devices for hazardous area

### Functional considerations

Using the following procedure the functional considerations checks whether the desired segment structure meets the basic requirements for transmission to the physical layer in IEC 61158-2.

*Step 1 – compilation of the functional characteristic values of the fieldbus components*

- Fieldbus power supply according FISCO model, Power Repeater KLD2-PR-Ex1.IEC1 (Pepperl+Fuchs):

$$U_S = 12.8 \text{ V (power supply voltage)}$$

$$I_S = 100 \text{ mA (power supply current)}$$

- Fieldbus line:

Cable type A

$$R_{WK} = 44 \text{ } \Omega/\text{km (effective resistance per unit length)}$$

- Fieldbus device Promag 53:

$$I_B = 12 \text{ mA (basic current)}$$

$$U_B = 9 \dots 32 \text{ V (perm. operating voltage)}$$

$$I_{FDE} = 0 \text{ mA (fault current)}$$

$$I_{\text{startup}} = 0 (< I_B)$$

- Fieldbus device Cerabar S:

$$\begin{aligned}
 I_B &= 10.5 \text{ mA (basic current)} \\
 U_B &= 9...32 \text{ V (perm. operating voltage)} \\
 I_{FDE} &= 0 \text{ mA (fault current)} \\
 I_{startup} &= 0 (< I_B)
 \end{aligned}$$

#### Step 2 – calculation of cable length and checking of network structure

An approved maximum length of 1000 meters has been set with the FISCO model for EEx ia IIC applications in order that the inductance and capacitance of the fieldbus cable can be ignored when used in hazardous area applications. This length comprises the length of the main cable and the total length of the drop cables together. In addition, it must be taken into account that the approved maximum length of a drop cable is 30 m.

#### Calculation of actual cable length $L_{SEG}$ :

$$\begin{aligned}
 L_{SEG} &= L_{main} + \sum L_{spurs} \\
 &= 580 \text{ m} + 80 \text{ m} \\
 &= \underline{\underline{660 \text{ m}}}
 \end{aligned}$$

Checking the conditions:

Consideration	Condition met?
$L_{SEG} < 1000 \text{ m}$ $660 \text{ m} < 1000 \text{ m}$	✓ Yes
$L_{spurs} < 30 \text{ m}$	✓ Yes

If one of the conditions is not met then the network structure must be revised.

#### Step 3 – current calculation

The number of field devices that can be connected to the H1 segment depends on the fieldbus power supply selected (supply voltage and supply current) and the current consumption of the field devices. Thus, the number of devices that can be connected is reduced if a field device consumes a basic current of more than 10 mA, e.g. 20 mA. By adding up the basic currents  $I_B$  of the field devices plus the response current in the event of a fault  $I_{FDE}$  for the FDE (**F**ault **D**isconnect **E**lectronics) and the current for the data modulation  $I_{MOD}$  (+9 mA) you can determine the minimum supply current that the fieldbus power supply must supply.

If, on switching on the device, the startup  $I_{startup}$  current is greater than the basic current, then the startup current must be taken into consideration in the calculation. The response current for the FDE ( $I_{FDE}$ ) is calculated for each field device from the difference between the maximum current in the event of a fault and the basic current. The field device with the greatest response current is taken into consideration in the current balance sheet.

Provided that no more than one FDE responds, the following condition must be taken into consideration in the calculation of the segment current  $I_{SEG}$ :

$$\begin{aligned}
 I_{SEG} &\leq I_S \\
 &\text{where} \\
 I_{SEG} &= \sum I_B + \max I_{FDE} + I_{MOD} + I_{startup}
 \end{aligned}$$

In the example the calculation formula results in the following segment current consumption  $I_{SEG}$ , where  $I_{FDE} = 0$ ,  $I_{startup} = 0$ , since the field devices used do not consume additional current in the event of a fault and the startup current is less than the bus current. In addition, the modulation current  $I_{MOD}$  for the installed bus power supply KLD2-PR-Ex1.IEC1 by Pepperl+Fuchs need not be considered since the value of the supply current  $I_S$  already includes this.

$$\begin{aligned}
 I_{SEG} &= \Sigma I_B \\
 &= \underline{\underline{79.5 \text{ mA}}}
 \end{aligned}$$

Checking the conditions:

Consideration	Condition met?
$I_{SEG} \leq I_S$ $79.5 \text{ mA} \leq 100 \text{ mA}$	✓ Yes

*Step 4 – Voltage at the last instrument*

The cable resistance causes a segment voltage drop, which is largest at the instrument farthest away from the bus power supply. For this reason it must be ensured that the minimum operating voltage of 9 V is available at this instrument. To make the overall considerations easier it is assumed that all the field devices FD (refer to Fig. 10) are connected at the end of the fieldbus line.

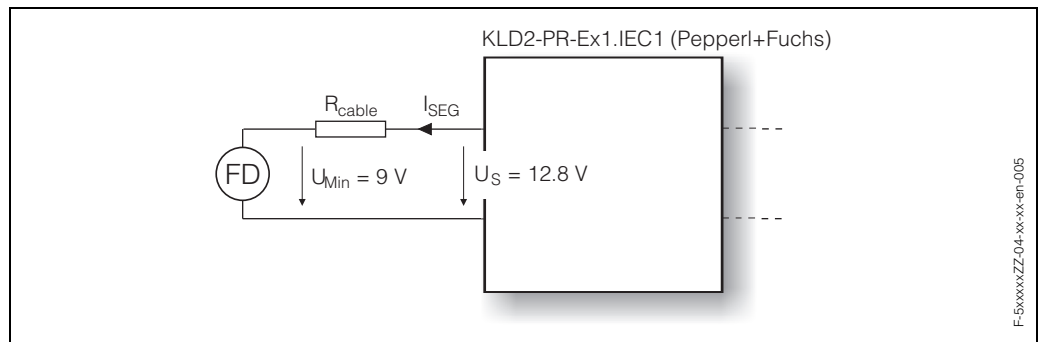


Fig. 10: Replacement circuit diagram

The resistance value  $R_{cable}$  must first be calculated in order to calculate the voltage drop caused by the fieldbus cable:

$$\begin{aligned}
 R_{cable} &= R_{WK} \times L_{SEG} \\
 &= 44 \text{ } \Omega/\text{km} \times 0.66 \text{ km} \\
 &= \underline{\underline{29 \text{ } \Omega}}
 \end{aligned}$$

Ohm's law is used to calculate the actual voltage  $U_{FG \text{ eff.}}$  at the last instrument:

$$\begin{aligned}
 U_{FG \text{ eff.}} &= U_S - (I_{SEG} \times R_{cable}) \\
 &= 12.8 \text{ V} - (79.5 \text{ mA} \times 29 \text{ } \Omega) \\
 &= 12.8 \text{ V} - 2.3 \text{ V} \\
 &= \underline{\underline{10.5 \text{ V}}}
 \end{aligned}$$

Checking the conditions:

Consideration	Condition met?
$U_{FG\text{ eff.}} \geq 9\text{ V}$	✓ Yes
$10.5\text{ V} \geq 9\text{ V}$	

**Final consideration:**

From a purely functional point of view the bus segment shown in the example can be operated based on the positive results.

**Technical safety considerations**

using variant Promag 53\*\*\*\_\*\*\*\*\*G

**Step 1 – compilation of technical values relevant to safety:**

*Fieldbus power supply (associated electrical apparatus)*

*FISCO Power Repeater KLD2-PR-Ex1.IEC1 (Pepperl+Fuchs):*

- Nominal values:

$$U_o = 15\text{ V}$$

$$I_o = 207.2\text{ mA}$$

$$P_o = 1.93\text{ W}$$

Described in the test certificate as “associated equipment”. Suitable for connection to a fieldbus system based on the FISCO model.

*Promag 53 (explosion protected electrical apparatus with intrinsically safe FF output):*

- Nominal values:

$$U_i = 30\text{ V}$$

$$I_i = 500\text{ mA}$$

$$P_i = 5.5\text{ W}$$

$$L_i = 10\text{ }\mu\text{H}$$

$$C_i = 5\text{ nF}$$

Suitable for connection to a fieldbus system based on the FISCO model.

*Cerabar S (explosion protected electrical apparatus with intrinsically safe FF output):*

- Nominal values FISCO:

$$U_i = 17.5\text{ V}$$

$$I_i = 500\text{ mA}$$

$$P_i = 5.5\text{ W}$$

$$L_i = 10\text{ }\mu\text{H}$$

$$C_i = 5\text{ nF}$$

Suitable for connection to a fieldbus system based on the FISCO model.

*Bus cable type A (shielded bus cable):*

- Nominal values:

$$R' = 24\text{ }\Omega/\text{km (loop resistance)}$$

$$C' = 82\text{ nF/km (capacitance per unit length)}$$

$$L' = 623\text{ }\mu\text{H/km (inductance per unit length)}$$

*Fieldbus connection KMD0-FT-Ex (Pepperl+Fuchs):*

• Nominal values:

$U_i$	=	24 V
$I_i$	=	280 mA
$P_i$	=	1.93 W
$R$	=	100 $\Omega$
$C$	=	1 $\mu\text{F}$

Suitable for connection to a fieldbus system based on the FISCO model.

## Step 2 – technical safety considerations acc. FISCO model

This step uses the existing data to check whether connecting the equipment is permissible from the point of view of technical safety. The conditions shown in the FISCO model apply to these safety considerations (see Page 13). First the functional data of the equipment used is compared. In this consideration it is crucial that the maximum output voltage and output current of the bus power supply does not exceed the permitted maximum input voltage and input current of the individual field devices. Here we consider possible error behaviour by the bus power supply that could result in the stated maximum values on the intrinsically safe sides.

Intrinsically safe equipment	Condition	Associated equipment FISCO Power Repeater KLD2-PR-Ex1.IEC1	Condition met?
<b>Promag 53</b>			
$U_i = 30 \text{ V}$	$\geq$	$U_o = 15 \text{ V}$	✓ Yes
$I_i = 500 \text{ mA}$	$\geq$	$I_o = 207.2 \text{ mA}$	✓ Yes
$P_i = 5.5 \text{ W}$	$\geq$	$P_o = 1.93 \text{ W}$	✓ Yes
As a further condition galvanic isolation must be provided due to the local supply			✓ Yes
<b>Cerabar S</b>			
$U_i = 17.5 \text{ V}$	$\geq$	$U_o = 15 \text{ V}$	✓ Yes
$I_i = 500 \text{ mA}$	$\geq$	$I_o = 207.2 \text{ mA}$	✓ Yes
$P_i = 5.5 \text{ W}$	$\geq$	$P_o = 1.93 \text{ W}$	✓ Yes
<b>Fieldbus connection KMD0-FT-Ex</b>			
$U_i = 24 \text{ V}$	$\geq$	$U_o = 15 \text{ V}$	✓ Yes
$I_i = 280 \text{ mA}$	$\geq$	$I_o = 207.2 \text{ mA}$	✓ Yes
$P_i = 1.93 \text{ W}$	$\geq$	$P_o = 1.93 \text{ W}$	✓ Yes

Since all the users are permissible for explosion group IIC and the corresponding parameters have been taken into consideration, the bus segment can be used for gases in explosion group IIC.

The permissible ambient temperature may be considered either individually for each device at the respective place of installation, or specified uniformly for the bus segment as a whole. In the latter case the lowest value of the ambient temperature applies.

Required temperature class	Intrinsically safe equipment	Maximum ambient temperature
T6	Cerabar S	40 °C
T5	Promag 53	50 °C (at 80 °C medium temperature)

In the next step is the verification of whether the installed bus components fulfil the conditions and limit values set in the FISCO model. This is simplified by ensuring the bus components correspond to the FISCO model. A detailed consideration of the safety-relevant nominal values is then not necessary.

Do bus components correspond to the FISCO model?	Condition met?
Power Repeater KLD2-PR-Ex1.IEC1	✓ Yes
Promag 53	✓ Yes
Cerabar S	✓ Yes
Fieldbus connection KMD0-FI-Ex	✓ Yes

The following conditions have been applied to the bus cable and network structure:

Bus cable:

Values	Condition	Limits acc. FISCO model	Condition met?
R'	> <	15 Ω/km 150 Ω/km	
C'	> <	80 nF/km 200 nF/km	
L'	> <	400 μH/km 1000 μH/km	
<b>Bus cable type A</b> R' = 24 Ω/km C' = 82 nF/km L' = 623 μH/km			✓ Yes

Network structure:

Consideration	Condition	Limits acc. FISCO model	Condition met?
Cable length including drop cables	≤	1000 m	
$L_{SEG} = 660$ m	≤	1000 m	✓ Yes
Drop cable length	≤	30 m	✓ Yes

#### Final consideration:

For the example shown, intrinsic safety according to the FISCO model can be proven.

## Device identification

Promag 53 FOUNDATION Fieldbus transmitter and W/P/H sensor

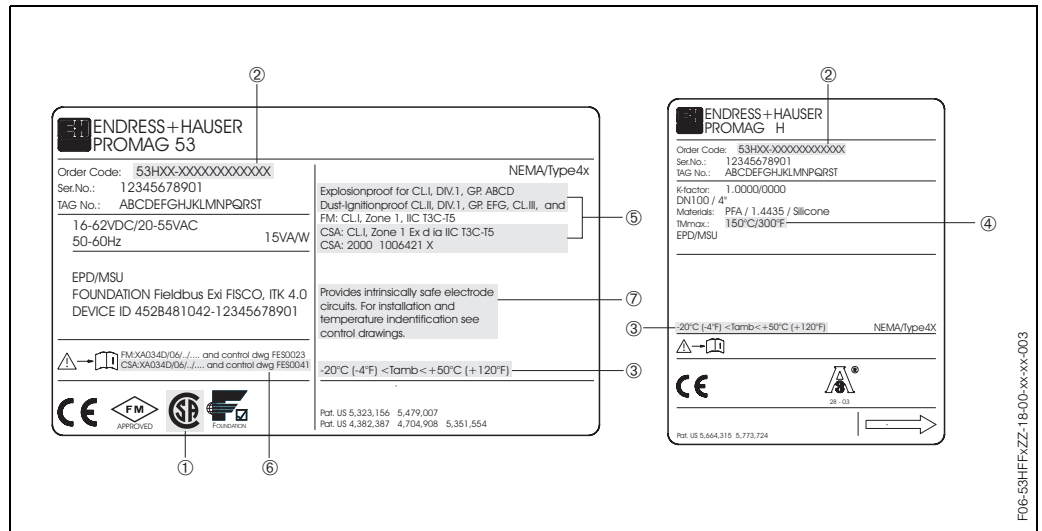


Fig. 11: Nameplate of transmitter and nameplate of sensor (example)

Key to nameplates (Figure 11)

No.	Meaning	No.	Meaning
①	Label of the notified body: Canadian Standards Association	⑤	Type of protection and explosion group for the Promag 53 FOUNDATION Fieldbus measuring system
②	Type code	⑥	Applicable Ex documentation
③	Ambient temperature range	⑦	Warning
④	Maximum medium temperature		

## Control drawings

Endress+Hauser Reinach hereby declares that the product is in conformity with the requirements of the CADADIAN STANDARDS ASSOCIATION.

**Hazardous Locations**  
Class I Division 1 Groups ABCD or Class I Zone 1 Groups IIC and Class II and III Division 1 Groups EFG

Promag 5. W / P Promag 5. H

**PROMAG 5. W / P / H**

Temperature table

Max. ambient temperature	Max. medium temperature depending temperature classes			
	T5	T4A	T4	T3C
50 °C / 122°F	50 °C / 122°F	110 °C / 230°F		
45 °C / 113°F	50 °C / 122°F	110 °C / 230°F	130 °C / 266°F	
40 °C / 104°F	50 °C / 122°F	110 °C / 230°F	130 °C / 266°F	150 °C / 302°F

Max. allowed medium temperature depending liner material

Liner material	Max. medium temperature
PU (polyurethan)	60 °C / 140°F
HG (hard rubber)	80 °C / 176°F
PTFE	130 °C / 266°F
PFA	150 °C / 302°F

Communication Options	Control Drawing
I/O option = F, H, J	See FES 0041 – 0001
I/O option = G, K	See FES 0041 – 0002
I/O option = S, T	See FES 0041 – 0004

**WARNING: SUBSTITUTION OF COMPONENTS MAY IMPAIR INTRINSIC SAFETY.**

Notes:

- Control room equipment shall not use or generate more than 250 V rms.
- Caution: Use supply wires suitable for 5 °C above ambient temperature, but at least for 80 °C / 176°F.
- Class II Group G: The surface temperature of the apparatus cannot exceed 165 °C / 329°F.
- Install per Canadian Electrical Code

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<b>CSA Control Drawing Div. 1 / Zone 1</b> Class I Zone 1				Gezeichnet 03.12.01 MDI
<b>PROMAG 5x compact version</b>				Geprüft
				Ex-geprüft 03.12.01 MDI
Flowtec AG, Kaegenstrasse 7, CH-4153 Reinach BL1, Postfach				Gesehen
<b>FES0041</b>				

**HAZARDOUS LOCATIONS**  
Cl. I Div. 1 Groups A,B,C,D  
Cl. I Zone 1 Group IIC  
Cl. I Div. 2 Group A,B,C,D  
Cl. I Zone 2 Group IIC  
Cl. II, III Div. 1 Group E,F,G

**NON HAZARDOUS LOCATIONS**

Notes:

**Intrinsically safe signal output:**

- Wire all intrinsically circuits per ISA RP 12.6. or in conduit per Canadian Electrical Code Part I
- WARNING: SUBSTITUTION OF COMPONENTS MAY IMPAIR INTRINSIC SAFETY.**
- Control room equipment may not use or generate more than 250 Vrms.

**PROMAG Type: 5\*\*\*\*-\*\*\*\*\*G**  
**Terminals 26, 27 (FOUNDATION Fieldbus):**  
Intrinsically safe circuit:

V <sub>max</sub> / U <sub>i</sub>	I <sub>max</sub> / I <sub>i</sub>	P <sub>max</sub> / P <sub>i</sub>	C <sub>i</sub>	L <sub>i</sub>
30 V	500 mA	5.5 W	≤ 5 nF	≤ 10 µH

Connect to entity approved associated apparatus with  
I<sub>sc</sub> or I<sub>0</sub> ≤ I<sub>max</sub> or I<sub>i</sub> and  
V<sub>oc</sub> or U<sub>0</sub> ≤ V<sub>max</sub> or U<sub>i</sub>  
(P<sub>0</sub> ≤ P<sub>max</sub> or P<sub>i</sub>)  
Cable parameters for Intrinsic Safety:  
C<sub>cable</sub> ≤ C<sub>0</sub> / C<sub>0</sub> - Σ C<sub>i</sub>  
L<sub>cable</sub> ≤ L<sub>0</sub> / L<sub>0</sub> - Σ L<sub>i</sub> or  
L/R<sub>cable</sub> ≤ L/R<sub>Associated Apparatus</sub> and L<sub>i</sub> of each I.S. apparatus ≤ 10 µH

Alternatively the intrinsically safe circuit ( Fieldbus Foundation ) can be connected according to the FISCO – Concept ( see 0041-0003 ).

**Nonintrinsically safe signal output:**

- Transmitter circuit wiring in accordance with Canadian Electrical Code.
- WARNING: EXPLOSION HAZARD - SUBSTITUTION OF COMPONENTS MAY IMPAIR SUITABILITY FOR CLASS I, DIVISION 1 OR CLASS I, ZONE 1.**
- Control room equipment may not use or generate over 250 Vrms.

PROMAG Type: 5\*\*\*\*-\*\*\*\*\*K  
**Terminals 26,27 (FIELDBUS FOUNDATION NON I.S.)**  
V ≤ 32 V, I = 10 mA

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<b>CSA Control Drawing Div. 1 / Zone 1</b> PROMAG 5. W / P / H				Gezeichnet 03.12.01 MDI
<b>Fieldbus Foundation I.S. installation</b>				Geprüft
				Ex-geprüft 03.12.01 MDI
Flowtec AG, Kaegenstrasse 7, CH-4153 Reinach BL1, Postfach				Gesehen
<b>FES0041 - 0002</b>				



**FISCO CONCEPT**  
 The FISCO Concept allows interconnection of intrinsically safe apparatus to associated apparatus not specially examined in such combination. The criteria for interconnection is that the voltage ( $U_i$  or  $V_{max}$ ), the current ( $I_i$  or  $I_{max}$ ), and the power ( $P_i$  or  $P_{max}$ ) which intrinsically safe apparatus can receive and remain intrinsically safe, considering faults, must be equal or greater than the voltage ( $U_o$  or  $V_{oc}$ ), the current ( $I_o$  or  $I_{sc}$ ) and the power ( $P_o$  or  $P_{max}$ ) levels which can be delivered by the associated apparatus, considering faults and applicable factors. In addition, the maximum unprotected capacitance ( $C_i$ ) and inductance ( $L_i$ ) of each apparatus (other than the termination) connected to the fieldbus must be less than or equal to 5 nF and 10  $\mu$ H respectively.  
 In each segment only one active device, normally the associated apparatus, is allowed to provide the necessary energy for the fieldbus system. The voltage  $U_o$  or  $V_{oc}$  of the associated apparatus is limited to a range of 14V to 24Vd.c. All other equipment connected to the bus cable has to be passive, meaning that they are not allowed to provide energy to the system, except a leakage current of 50 $\mu$ A for each connected device. Separately powered equipment needs a galvanic isolation to assure that the intrinsically safe fieldbus circuit remains passive.  
 The cable used to interconnect the devices needs to have the parameter in the following range:

Loop Resistance R' : 15...150 Ohm/km  
 Inductance per unit length L' : 0.4...1 mH/km  
 Capacitance per unit length C' : 80...200 nF

$C' = C' \text{ line/line} + 0.5 C' \text{ line/screen}$ , if both lines are floating, or  
 $C' = C' \text{ line/line} + C' \text{ line/screen}$ , if the screen is connected to one line  
 Length of trunk cable:  $\leq 1000$  m  
 Length of spur cable:  $\leq 30$  m  
 Length of splice:  $\leq 1$  m

At each end of the trunk cable an approved infallible line termination with following parameters is suitable:  
 $R = 90...100 \text{ Ohm}$        $C = 0...2.2 \mu\text{F}$   
 One of the allowed terminations might already be integrated in the associated apparatus. The number of passive apparatus connected to the bus segment is not limited due to I. S. reasons. If the above rules are respected, up to a total length of 1000 m (sum of trunk and all spur cables), the inductance and the capacitance of the cable will not impair the intrinsic safety of the installation.

**Notes:**  
**Intrinsically safe Class I, Div.1, Groups A,B,C,D**  
 1. Approved associated apparatus must be installed in accordance with manufacturers instructions.  
 2. CSA approved associated apparatus must meet the following parameters:  
 $U_o$  or  $V_{oc} \leq U_i$  ( $V_{max}$ ) and  $I_o$  or  $I_{sc} \leq I_i$  ( $I_{max}$ ) and  $P_o$  or  $P_{max} \leq P_i$  ( $P_{max}$ )  
 3. The maximum non-hazardous area voltage must not exceed 250V  
 4. The installation must be in accordance with the Canadian Electrical Code  
 5. Multiple earthing of screen is allowed only, if high integrity equipotential system is realized between the points of bonding (see drawing No. FES 0014).  
 6. Caution: Use only supply wires suitable for 5°C above surrounding temperature.  
 7. Warning: Substitution of components may impair intrinsic safety.  
 8. The polarity for connection PA+ (26) and PA- (27) is of no importance due to an internal rectifier.

**HAZARDOUS (CLASSIFIED) LOCATION**  
 Class I, Division 1, Groups A,B,C,D  
 Class II, Division 1, Groups E,F,G  
 Class III, Division 1

**NONHAZARDOUS LOCATION**

Anderungen:	<table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td style="width: 5%;">A</td><td style="width: 20%;">03.12.01/MDI</td><td style="width: 5%;">F</td><td style="width: 10%;"></td><td style="width: 60%;">Alle gesetzlichen Urheberrechte vorbehalten.</td></tr> <tr><td>B</td><td></td><td>G</td><td></td><td>Diese Zeichnung darf ohne unsere</td></tr> <tr><td>C</td><td></td><td>H</td><td></td><td>Genehmigung weder vervielfältigt werden noch</td></tr> <tr><td>D</td><td></td><td>I</td><td></td><td>driften Personen und Konkurrenzfirmen</td></tr> <tr><td>E</td><td></td><td>K</td><td></td><td>zugänglich gemacht werden.</td></tr> </table>	A	03.12.01/MDI	F		Alle gesetzlichen Urheberrechte vorbehalten.	B		G		Diese Zeichnung darf ohne unsere	C		H		Genehmigung weder vervielfältigt werden noch	D		I		driften Personen und Konkurrenzfirmen	E		K		zugänglich gemacht werden.	Ersetzt durch: Ersteller: FES / ID 1077 File: M:ZEICHNUNG\FES0041\011203C.DOC
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<b>CSA Control Drawing Div. 1 / Zone 1</b> <b>PROMAG 5. W / P / H</b> <b>Intrinsically safe PROFIBUS PA</b> <b>FISCO-Concept</b>																											
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**Supplementary  
documentation**

TI 046D/06  
TI 047D/06  
TI 048D/06

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